Town of Simsbury Office of Community Planning and Development - Zoning Commission A pplication
DATE: July 6, 2022 FEE: \$540.00 CK #: 1669 APP #:
PROPERTY ADDRESS: 230 Bushy Hill Road
NAME OF OWNER: The Ethel Walker School attn: Beth McWilliams, CFO/CEO
MAILING ADDRESS: 230 Bushy Hill Road, Simsbury CT 06070
EMAIL ADDRESS:
NAME OF AGENT: Same as owner
MAILING ADDRESS:
EMAIL ADDRESS: TELEPHONE #
ZONING DISTRICT: R-40 LOT AREA: 106 SQ FT ACRE
Does this site have wetlands? YES INO Have you applied for a wetlands permit? YES INO
REQUESTED ACTION (PLEASE CHECK APPROPRIATE BOX):
ZONE CHANGE : The applicant hereby requests that said premises be changed from zone to zone
TEXT AMENDMENT: Please attach proposed changes, including Articles and Sections, and purposes.
SPECIAL EXCEPTION: The applicant hereby requests a public hearing pursuant to Article, Section
SITE PLAN APPROVAL: The applicant hereby requests
PRELIMINARY FINAL SITE PLAN AMENDMENT pursuant to Article 5, Section
SIGN PERMIT
OTHER (PLEASE EXPLAIN):

NOTE: Each application must fully comply with the requirements of the Zoning Regulations prior to receipt by the Commission. <u>Each application for zone change and/or special exception shall include a list of names and addresses of</u> abutting property owners and all property owners within 100 feet of the subject site.

A check payable to the Town of Simsbury must accompany this <u>original signed and dated</u> application. <u>Six (6) complete</u> (folded) sets of plans and eleven (11) copies of the completed application and correspondence must also be included. If you have a PDF of your plans, we would appreciate a copy of that sent to <u>lbarkowski@simsbury-ct.gov</u>, as well.

n'ul 6/27/22

Signature of Owner

Date

Signature of Agent

Date

Telephone (860) 658-3245 F acsimile (860) 658-3206 www.simsbury-ct.gov

933 Hopmeadow Street Simsbury, CT 06070

GENERAL NOTES

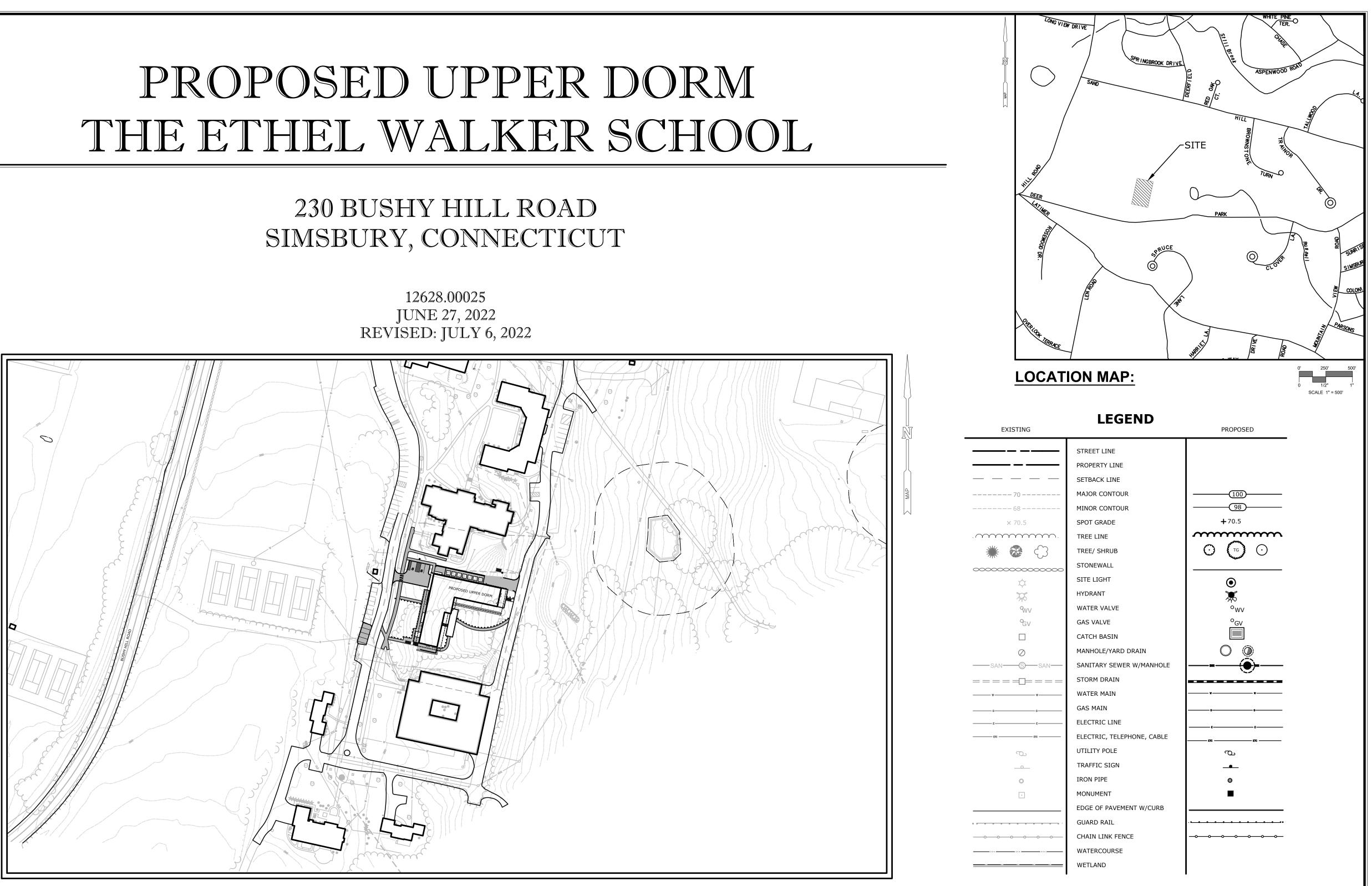
- 1. PROPERTY AND TOPOGRAPHIC INFORMATION COMPILED FROM 1.1.1. MAP ENTITLED "TOPOGRAPHIC SURVEY, PREPARED FOR THE THEL WALKER SCHOOL, 230 BUSHY HILL ROAD, SIMSBURY, CONNECTICUT," SCALE: 1"=20', DATE: 3/20/2022, REVISED: 4/05/2022, PREPARED BY: SLR INTERNATIONAL CORPORATION AERIAL MAPPING PREPARED BY GOLDEN AERIAL SURVEYS
- AVAILABLE TOWN OF SIMSBURY GIS MAPPING 1.1.3. 2. NORTH ARROW, BEARINGS AND COORDINATES ARE BASED UPON THE CONNECTICUT COORDINATE SYSTEM (NAD 1983). ELEVATIONS, CONTOURS AND
- BENCH MARK ARE BASED UPON (NAVD 1988) 3. INFORMATION REGARDING THE LOCATION OF EXISTING UTILITIES HAS BEEN BASED UPON AVAILABLE INFORMATION AND MAY BE INCOMPLETE, AND WHERE SHOWN SHOULD BE CONSIDERED APPROXIMATE. THE LOCATION OF ALL EXISTING UTILITIES SHOULD BE CONFIRMED PRIOR TO BEGINNING
- CONSTRUCTION. CALL <u>"CALL BEFORE YOU DIG</u>", 1-800-922-4455. ALL UTILITY LOCATIONS THAT DO NOT MATCH THE VERTICAL OR HORIZONTAL CONTROL SHOWN ON THE PLANS SHALL IMMEDIATELY BE BROUGHT TO THE ATTENTION OF THE ENGINEER FOR RESOLUTION. 4. SLR INTERNATIONAL CORPORATION ACCEPTS NO RESPONSIBILITY FOR THE ACCURACY OF MAPS AND DATA WHICH HAVE BEEN SUPPLIED BY OTHERS.
- 5. ALL UTILITY SERVICES ARE TO BE UNDERGROUND. THE EXACT LOCATION, MEANS OF CONSTRUCTION, AND SIZE OF ELECTRIC, TELEPHONE, AND CABLE TELEVISION ARE TO BE DETERMINED BY THE RESPECTIVE UTILITY COMPANIES.
- 6. ALL DIMENSIONS AND ELEVATIONS SHALL BE VERIFIED IN THE FIELD PRIOR TO CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER.
- 7. SEDIMENT AND EROSION CONTROL MEASURES AS DEPICTED ON THESE PLANS AND DESCRIBED WITHIN THE SEDIMENT AND EROSION CONTROL NARRATIVE SHALL BE IMPLEMENTED AND MAINTAINED UNTIL PERMANENT COVER AND STABILIZATION IS ESTABLISHED. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL CONFORM TO THE "GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL, CONNECTICUT - 2002". AND IN ALL CASES BEST MANAGEMENT PRACTICES SHALL PREVAIL
- 8. ALL DISTURBED AREAS SHALL RECEIVE A MINIMUM OF 4" TOPSOIL, AND BE SEEDED WITH GRASS, AS SHOWN ON THE PLANS.
- 9. ALL PROPOSED CONTOURS AND SPOT ELEVATIONS INDICATE FINISHED GRADE.
- 10. ALL CONSTRUCTION MATERIALS AND METHODS SHALL CONFORM TO THE TOWN OF SIMSBURY REQUIREMENTS AND TO THE APPLICABLE SECTIONS OF THE STATE OF CONNECTICUT DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS FOR ROADS, BRIDGES, AND INCIDENTAL CONSTRUCTION, FORM 818 AND ADDENDUMS.
- 11. THE PLANS REQUIRE A CONTRACTOR'S WORKING KNOWLEDGE OF LOCAL, MUNICIPAL, WATER AUTHORITY, AND STATE CODES FOR UTILITY SYSTEMS. ANY CONFLICTS BETWEEN MATERIALS AND LOCATIONS SHOWN, AND LOCAL REQUIREMENTS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO THE EXECUTION OF WORK. THE ENGINEER WILL NOT BE HELD LIABLE FOR COSTS INCURRED TO IMPLEMENT OR CORRECT WORK WHICH DOES NOT CONFORM TO LOCAL CODE.
- ALL FUEL, OIL, PAINT, OR OTHER HAZARDOUS MATERIALS USED DURING CONSTRUCTION SHOULD BE STORED IN A SECONDARY CONTAINER AND REMOVED TO A LOCKED INDOOR AREA WITH AN IMPERVIOUS FLOOR DURING NON-WORK HOURS.
- 13. COMPLIANCE WITH THE PERMIT CONDITIONS IS THE RESPONSIBILITY OF BOTH THE CONTRACTOR AND THE PERMITTEE. 14. A PRE-CONSTRUCTION MEETING, SCHEDULED THROUGH THE TOWN PLANNING DEPARTMENT, SHALL BE HELD PRIOR TO CONSTRUCTION.

ZONING DATA TABLE

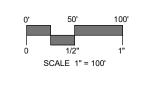
EXISTING ZONE: R-40

REQUIRED
40,000 SQ. FT. (0.92 ACRES)
200 FT. MINIMUM
50 FT. MINIMUM
40 FT. MINIMUM
50 FT. MINIMUM
35 FT. MAXIMUM





PROJECT SITE VICINITY MAP:



PREPARED BY:

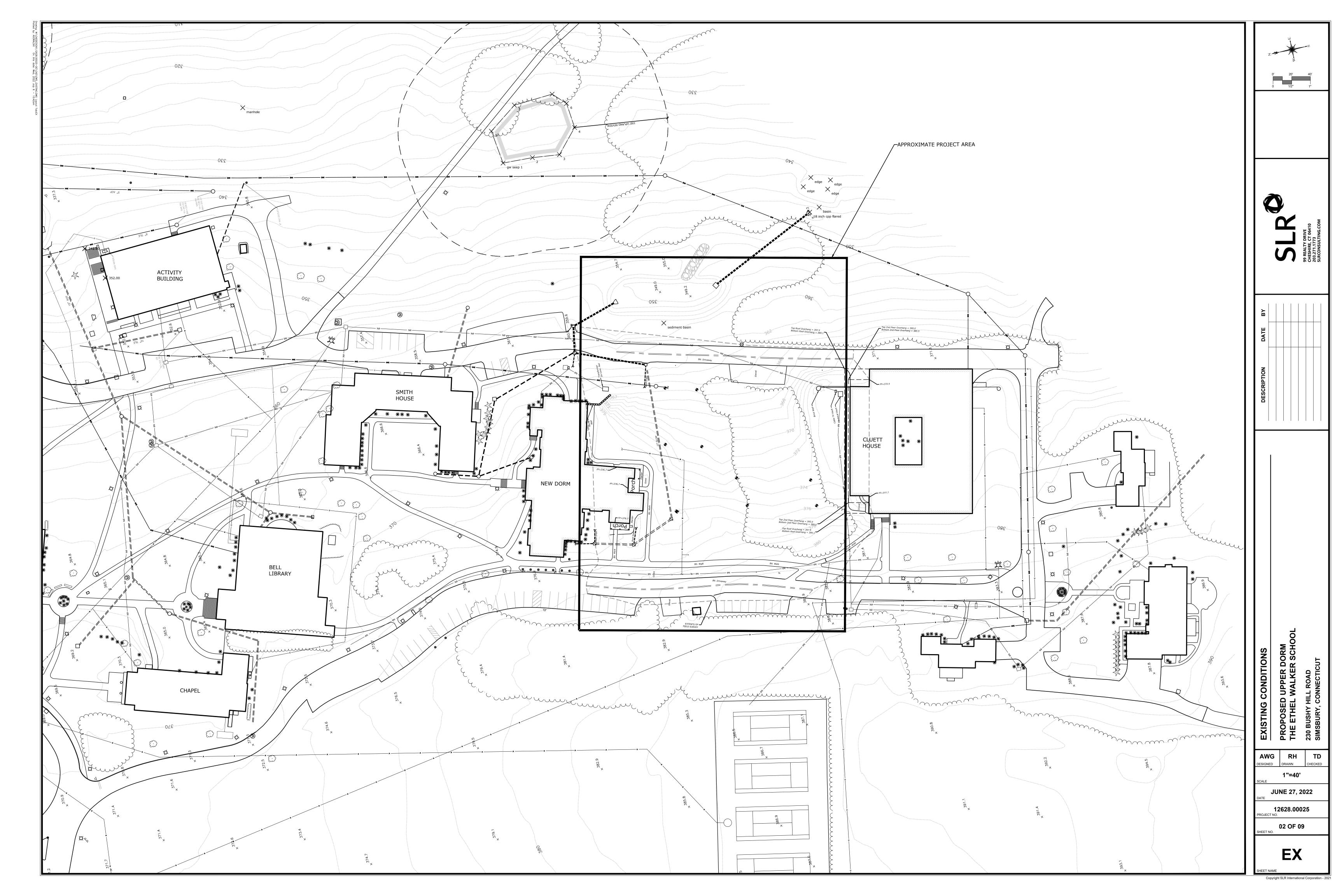


PREPARED FOR:

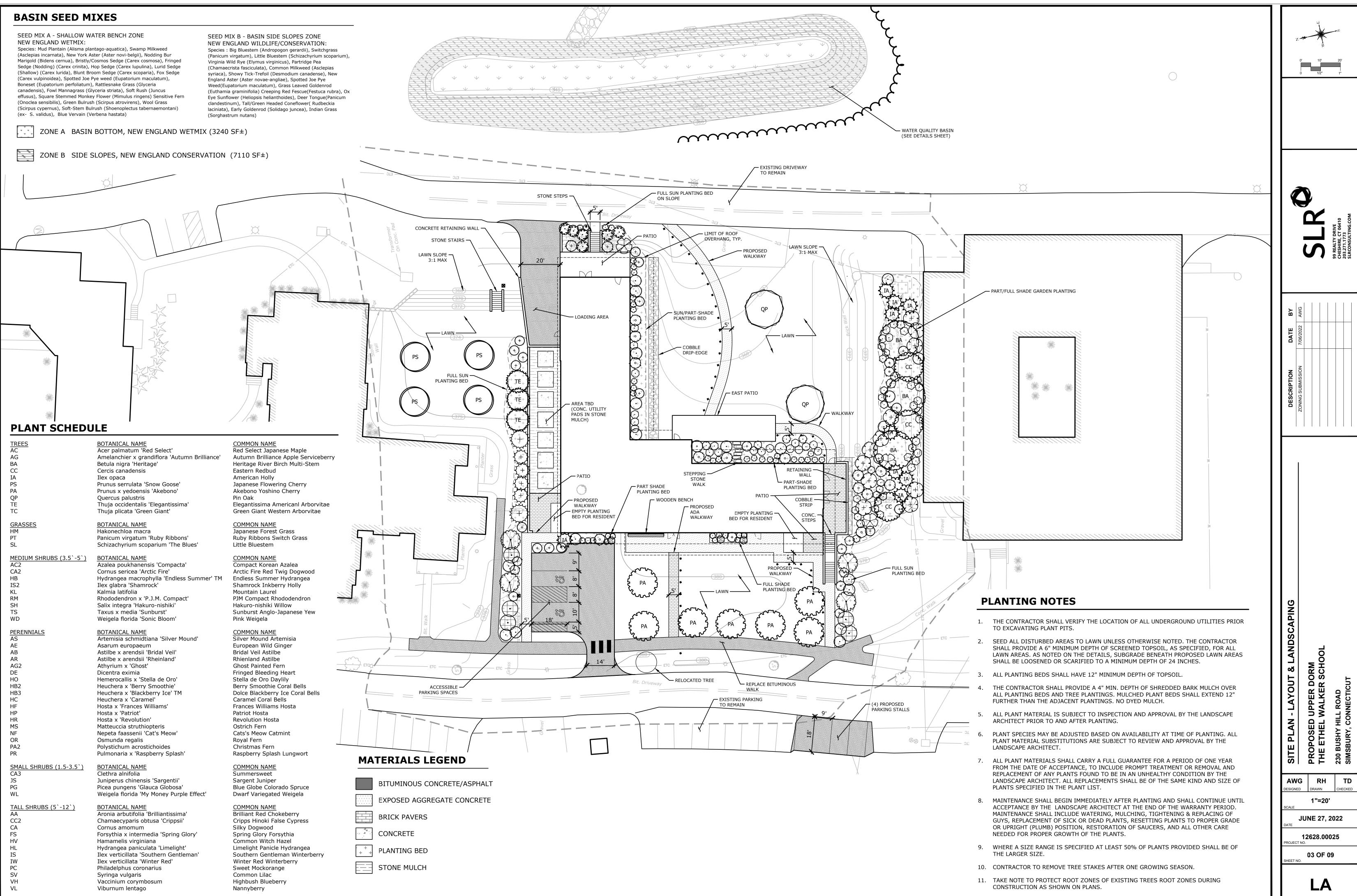
THE ETHEL WALKER SCHOOL 230 BUSHY HILL ROAD SIMSBURY, CONNECTICUT 06070

LIST OF DRAWINGS

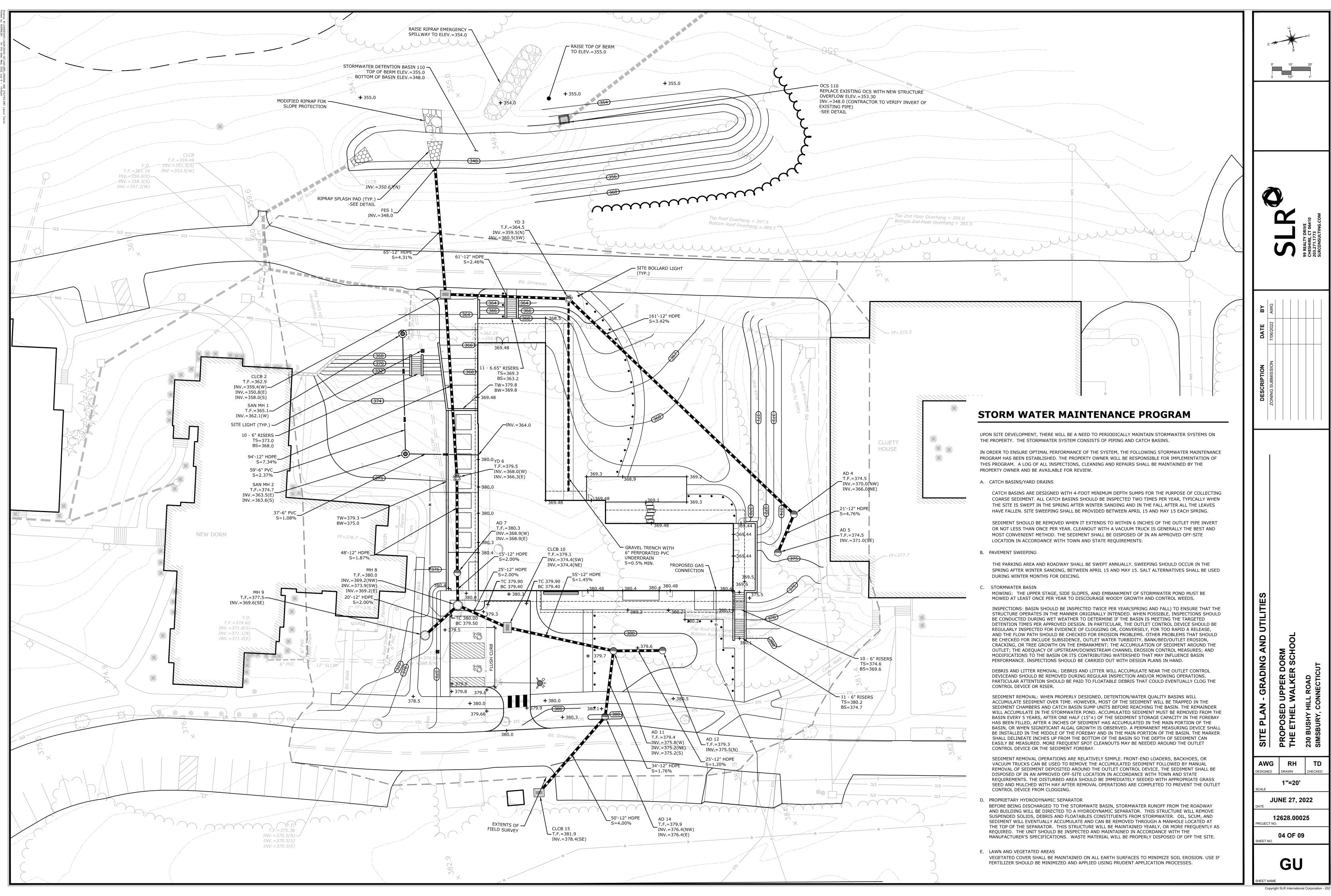
NO.	NAME	TITLE
01		TITLE SHEET
02	EX	EXISTING CONDITIONS
03	LA	SITE PLAN - LAYOUT AND LANDSCAPING
04	GU	SITE PLAN - GRADING AND UTILITIES
05	SE-1	SEDIMENT AND EROSION CONTROL PLAN
06	SE-2	SEDIMENT AND EROSION CONTROL DETAILS AND SPECIFICATIONS
07	SD-1	SITE DETAILS
08	SD-2	SITE DETAILS
09	SD-3	SITE DETAILS

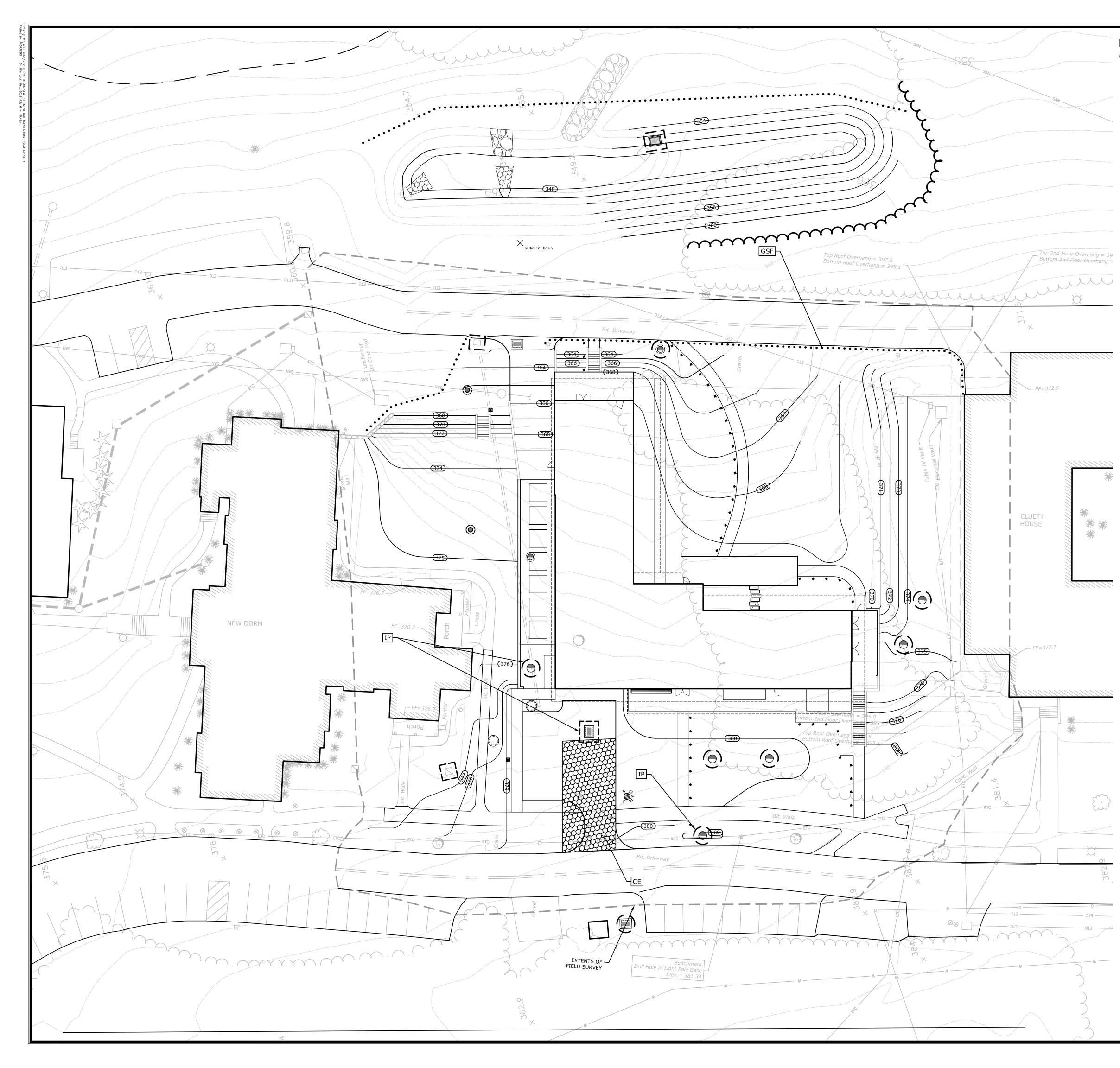






	1
Copyright SLR International Corporation - 2027	Ī





EROSION CONTROL NOTES CONTRACTOR RESPONSIBILITIES

- 1. SEDIMENT AND EROSION CONTROLS SHALL BE INSPECTED AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL AMOUNT OF 0.5 INCH OR GREATER. A LOG OF SUCH INSPECTIONS SHALL BE MAINTAINED AT THE SITE.
- 2. THE SEDIMENT AND EROSION CONTROL PLAN SHALL BE MODIFIED BY THE CONTRACTOR AT THE DIRECTION OF THE ENGINEER AND THE TOWN'S DESIGNATED REPRESENTATIVE AS NECESSITATED BY CHANGING SITE CONDITIONS
- 3. INSPECTION OF THE SITE FOR EROSION SHALL CONTINUE FOR A PERIOD OF THREE MONTHS AFTER COMPLETION WHEN RAINFALLS OF ONE INCH OR MORE OCCUR.
- 4. ALL DEWATERING WASTE WATERS SHALL BE DISCHARGED IN A MANNER WHICH MINIMIZES THE DISCOLORATION OF THE RECEIVING WATERS.
- 5. THE SITE SHOULD BE KEPT CLEAN OF LOOSE DEBRIS, LITTER, AND BUILDING MATERIALS SUCH THAT NONE OF THE ABOVE ENTER WATERS OR WETLANDS.
- 6. A COPY OF ALL PLANS AND REVISIONS, AND THE SEDIMENT AND EROSION CONTROL PLAN SHALL BE MAINTAINED ON-SITE AT ALL TIMES DURING CONSTRUCTION.
- 7. ALL CATCH BASIN SUMPS SHOULD BE INSPECTED AFTER CONSTRUCTION COMPLETION AND SEDIMENT REMOVED. THE SEDIMENT SHALL BE DISPOSED OF IN AN APPROVED LOCATION.
- 8. MONITORING REPORTS SHALL BE PROVIDED TO THE TOWN OF FARMINGTON AND CONTRACTOR EVERY TWO WEEKS AND FOR ANY STORM OVER $\frac{1}{2}$ INCH. REPAIRS SHALL BE MADE WITHIN 24 HOURS AFTER REPORTING.
- 9. PROPOSED DETENTION BASINS SHALL NOT BE UTILIZED AS TEMPORARY SEDIMENTATION BASINS DURING CONSTRUCTION.

SOIL EROSION AND SEDIMENT CONTROL NARRATIVE

SEDIMENT AND EROSION CONTROL MEASURES AS DEPICTED ON THESE PLANS AND DESCRIBED WITHIN THE SEDIMENT AND EROSION CONTROL NARRATIVE SHALL BE IMPLEMENTED AND MAINTAINED UNTIL PERMANENT COVER AND STABILIZATION IS ESTABLISHED. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL CONFORM TO THE "GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL, CONNECTICUT - 2002, TOWN OF SIMSBURY STANDARDS, AND IN ALL CASES BEST MANAGEMENT PRACTICES SHALL PREVAIL.

- 1.<u>PURPOSE AND DESCRIPTION OF PROJECT</u> A.) CONSTRUCTION OF A NEW DORMITORY BUILDING.
- B.) DISTURBED AREA: ± 1.6 ACRES

2.IDENTIFICATION OF EROSION AND SEDIMENT CONTROL CONCERNS A.) CUTS AND FILLS ASSOCIATED WITH CONSTRUCTION.

3.<u>IDENTIFICATION OF OTHER POSSIBLE PERMITS</u> THE PERMITS REQUIRED FOR THE PROJECT ARE LOCAL INLAND WETLANDS, AND PLANNING AND ZONING PERMITS.

4.<u>RESPONSIBLE PARTY</u> MS. BETH MCWILLIAMS THE ETHEL WALKER SCHOOL 230 BUSHY HILL ROAD

SIMSBURY, CT 06070

EROSION CONTROL LEGEND

CECONSTRUCTION ENTRANCEImage: CEImage: Ce

STK

--- sw Straw Wattles

TEMPORARY SOIL STOCKPILE AREA SURROUNDED WITH SEDIMENT FILTER FENCE

Z - 4	10' 1/2"	20' 1"
	SLR	99 REALTY DRIVE CHESHIRE, CT 06410 203.271.1773 SLRCONSULTING.COM
DATE BY		
DESCRIPTION		
	PROPOSED UPPER DORM	
	RH DRAWN 1"=20' UNE 27, 2	
DATE PROJECT NO SHEET NO.	2628.000 	
SHEET NAME	SE-	1

Copyright SLR International Corporation - 2021

THESE GUIDELINES SHALL APPLY TO ALL WORK CONSISTING OF ANY AND ALL TEMPORARY AND/OR PERMANENT MEASURES TO CONTROL WATER POLLUTION AND SOIL EROSION, AS MAY BE REQUIRED. DURING THE CONSTRUCTION OF THE PROJECT. IN GENERAL, ALL CONSTRUCTION ACTIVITIES SHALL PROCEED IN SUCH A MANNER SO AS NOT TO POLLUTE ANY WETLANDS, WATERCOURSE, WATERBODY, AND CONDUIT CARRYING WATER, ETC. THE CONTRACTOR SHALL LIMIT, INSOFAR AS POSSIBLE, THE SURFACE AREA OF EARTH MATERIALS EXPOSED BY CONSTRUCTION METHODS AND IMMEDIATELY PROVIDE PERMANENT AND TEMPORARY POLLUTION CONTROL MEASURES TO PREVENT CONTAMINATION OF ADJACENT WETLANDS, WATERCOURSES, AND WATERBODIES, AND TO PREVENT, INSOFAR AS POSSIBLE, EROSION ON THE SITE.

LAND GRADING

GENERAL:

THE RESHAPING OF THE GROUND SURFACE BY EXCAVATION AND FILLING OR A COMBINATION OF BOTH, TO OBTAIN PLANNED GRADES, SHALL PROCEED IN

- ACCORDANCE WITH THE FOLLOWING CRITERIA: a. THE CUT FACE OF EARTH EXCAVATION SHALL NOT BE STEEPER THAN TWO
- HORIZONTAL TO ONE VERTICAL (2:1). b. THE PERMANENT EXPOSED FACES OF FILLS SHALL NOT BE STEEPER THAN TWO
- HORIZONTAL TO ONE VERTICAL (2:1). c. THE CUT FACE OF ROCK EXCAVATION SHALL NOT BE STEEPER THAN ONE
- HORIZONTAL TO FOUR VERTICAL (1:4). PROVISION SHOULD BE MADE TO CONDUCT SURFACE WATER SAFELY TO STORM DRAINS TO PREVENT SURFACE RUNOFF FROM DAMAGING CUT FACES AND FILL SLOPES.
- e. EXCAVATIONS SHOULD NOT BE MADE SO CLOSE TO PROPERTY LINES AS TO ENDANGER ADJOINING PROPERTY WITHOUT PROTECTING SUCH PROPERTY FROM
- EROSION, SLIDING, SETTLING, OR CRACKING. NO FILL SHOULD BE PLACED WHERE IT WILL SLIDE OR WASH UPON THE
- PREMISES OF ANOTHER OWNER OR UPON ADJACENT WETLANDS, WATERCOURSES, OR WATERBODIES.
- g. PRIOR TO ANY REGRADING, A STABILIZED CONSTRUCTION ENTRANCE SHALL BE PLACED AT THE ENTRANCE TO THE WORK AREA IN ORDER TO REDUCE MUD AND OTHER SEDIMENTS FROM LEAVING THE SITE.

TOPSOILING GENERAL:

- TOPSOIL SHALL BE SPREAD OVER ALL EXPOSED AREAS IN ORDER TO PROVIDE A SOIL MEDIUM HAVING FAVORABLE CHARACTERISTICS FOR THE ESTABLISHMENT, GROWTH, AND MAINTENANCE OF VEGETATION.
- UPON ATTAINING FINAL SUBGRADES, SCARIFY SURFACE TO PROVIDE A GOOD BOND WITH TOPSOIL. REMOVE ALL LARGE STONES, TREE LIMBS, ROOTS AND CONSTRUCTION DEBRIS
- APPLY SOIL AMENDMENTS AS FOLLOWS: LIME: ACCORDING TO SOIL TEST OR AT THE RATE OF 2 TONS PER ACRE.
- ROCK DUST: ACCORDING TO SOIL TEST OR AT THE RATE OF 2 TONS PER ACRE

MATERIAL:

- TOPSOIL SHOULD HAVE PHYSICAL, CHEMICAL, AND BIOLOGICAL CHARACTERISTICS FAVORABLE TO THE GROWTH OF PLANTS. TOPSOIL SHOULD HAVE A SANDY OR LOAMY TEXTURE
- TOPSOIL SHOULD BE RELATIVELY FREE OF SUBSOIL MATERIAL AND MUST BE FREE OF LARGE STONES, LUMPS OF SOIL, ROOTS, TREE LIMBS, TRASH, OR CONSTRUCTION DEBRIS. IT SHOULD BE FREE OF ROOTS OR RHIZOMES SUCH AS THISTLE, NUTGRASS,
- AND QUACKGRASS. AN ORGANIC MATTER CONTENT OF SIX PERCENT (6%) IS REQUIRED. AVOID LIGHT COLORED SUBSOIL MATERIAL. SOLUBLE SALT CONTENT OF LESS THAN 400 PPM IS REQUIRED.
- THE TOPSOIL SHALL BE WARRANTED BY SELLER TO BE FREE OF DETECTABLE RESIDUES OF CHEMICAL PESTICIDES, HERBICIDES, PETROLEUM PRODUCTS, OR OTHER UNSUITABLE TOXINS.

APPLICATION:

AVOID SPREADING WHEN TOPSOIL IS WET OR FROZEN. SPREAD TOPSOIL UNIFORMLY TO A DEPTH OF AT LEAST FOUR INCHES (4"), OR TO THE DEPTH SHOWN ON THE LANDSCAPING PLANS.

TEMPORARY VEGETATIVE COVER

TEMPORARY VEGETATIVE COVER SHALL BE ESTABLISHED ON ALL UNPROTECTED AREAS THAT PRODUCE SEDIMENT, AREAS WHERE FINAL GRADING HAS BEEN COMPLETED, AND AREAS WHERE THE ESTIMATED PERIOD OF BARE SOIL EXPOSURE IS LESS THAN 12 MONTHS. TEMPORARY VEGETATIVE COVER SHALL BE APPLIED IF AREAS WILL NOT BE PERMANENTLY SEEDED BY SEPTEMBER 1.

GENERAL:

- INSTALL REQUIRED SURFACE WATER CONTROL MEASURES. REMOVE LOOSE ROCK, STONE, AND CONSTRUCTION DEBRIS FROM AREA. APPLY SOIL AMENDMENTS AS FOLLOWS:
- LIME: ACCORDING TO SOIL TEST OR AT THE RATE OF 1 TONS PER ACRE. ROCK DUST: ACCORDING TO SOIL TEST OR AT THE RATE OF 1 TONS PER ACRE UNLESS HYDROSEEDED, WORK IN LIME TO A DEPTH OF 4 INCHES WITH A DISK OR
- ANY SUITABLE EQUIPMENT. DO NOT WORK FINISHED COMPOST INTO THE SOIL -APPLY IT EVENLY TO SOIL SURFACE AS A SEED BED. TILLAGE SHOULD ACHIEVE A REASONABLY UNIFORM LOOSE SEEDBED. WORK ON CONTOUR IF SITE IS SLOPING.

SITE PREPARATION:

- SELECT APPROPRIATE SPECIES FOR THE SITUATION. NOTE RATES AND SEEDING
- DATES (SEE VEGETATIVE COVER SELECTION & MULCHING) APPLY SEED UNIFORMLY ACCORDING TO THE RATE INDICATED BY BROADCASTING,
- DRILLING, OR HYDRAULIC APPLICATION. UNLESS HYDROSEEDED, COVER RYEGRASS SEEDS WITH NOT MORE THAN 1/4 INCH OF
- SOIL USING SUITABLE EQUIPMENT MULCH IMMEDIATELY AFTER SEEDING IF REQUIRED. (SEE VEGETATIVE COVER SELECTION & MULCHING SPECIFICATION BELOW.) APPLY STRAW AND ANCHOR TO SLOPES GREATER THAN 3%%% OR WHERE NEEDED.

PERMANENT VEGETATIVE COVER

GENERAL:

PERMANENT VEGETATIVE COVER SHALL BE ESTABLISHED AS VARIOUS SECTIONS OF THE PROJECT ARE COMPLETED IN ORDER TO STABILIZE THE SOIL, REDUCE DOWNSTREAM DAMAGE FROM SEDIMENT AND RUNOFF, AND TO ENHANCE THE AESTHETIC NATURE OF THE SITE. IT WILL BE APPLIED TO ALL CONSTRUCTION AREAS SUBJECT TO EROSION WHERE FINAL GRADING HAS BEEN COMPLETED AND A PERMANENT COVER IS NEEDED.

SITE PREPARATION:

- INSTALL REQUIRED SURFACE WATER CONTROL MEASURES.
- REMOVE LOOSE ROCK, STONE, AND CONSTRUCTION DEBRIS FROM AREA. PERFORM ALL PLANTING OPERATIONS PARALLEL TO THE CONTOURS OF THE SLOPE.
- APPLY TOPSOIL AS INDICATED ELSEWHERE HEREIN.
- APPLY SOIL AMENDMENTS AS FOLLOWS:
- LIME: ACCORDING TO SOIL TEST OR AT THE RATE OF 1 TONS PER ACRE. ROCK DUST: ACCORDING TO SOIL TEST OR AT THE RATE OF 1 TONS PER ACRE 6. UNLESS HYDROSEEDED, WORK IN LIME TO A DEPTH OF 4 INCHES WITH A DISK OR ANY SUITABLE EQUIPMENT. DO NOT WORK FINISHED COMPOST

VEGETATED COVER SELECTION AND MULCHING

TEMPORARY VEGETATIVE COVER:

PERENNIAL RYEGRASS 5 LBS./1,000 SQ.FT. (LOLIUM PERENNE) DUTCH WHITE CLOVER (TRIFOLIUM REPENS) 1/4 LBS PER 1000 SF. OR 6LBS/AC.

* PERMANENT VEGETATIVE COVER: DUTCH WHITE CLOVER 30%

BARON KENTUCKY BLUEGRASS 30% JAMESTOWN II CHEWINGS FESCUE 20%

PALMER PERENNIAL RYEGRASS 20%

NEW ENGLAND EROSION CONTROL/R3ESOTRATION MIX FOR MOIST SITES AT 1/8 LB PER 1000 S.F. FOR 5 LBS/AC.

NEW ENGLAND SHOWY WILD FLOW MIX AT 1/16 LB PER 1000 S.F. OR 2 LBS/AC

* LOFTS - "TRIPLEX GENERAL" MIX OR APPROVED EQUAL. RECOMMENDED RATE/TIME SEEDING

SPRING SEEDING: 4/1 to 5/31 FALL SEEDING: 8/16 to 10/15

TEMPORARY MULCHING:

STRAY 70-90 LBS./1,000 SQ.FT. (TEMPORARY VEGETATIVE AREAS) WOOD FIBER IN HYDROMULCH SLURRY 25-50 LBS./1,000 SQ. FT.

- ESTABLISHMENT: SMOOTH AND FIRM SEEDBED WITH CULTIPACKER OR OTHER SIMILAR EQUIPMENT
- PRIOR TO SEEDING (EXCEPT WHEN HYDROSEEDING). SELECT ADAPTED SEED MIXTURE FOR THE SPECIFIC SITUATION. NOTE RATES AND 2. THE SEEDING DATES (SEE VEGETATIVE COVER SELECTION & MULCHING SPEC. BELOW)
- 3. APPLY SEED UNIFORMLY ACCORDING TO RATE INDICATED, BY BROADCASTING, DRILLING, OR HYDRAULIC APPLICATION.
- COVER GRASS AND LEGUME SEED WITH NOT MORE THAN 1/4 INCH OF SOIL WITH SUITABLE EQUIPMENT (EXCEPT WHEN HYDROSEEDING). MULCH IMMEDIATELY AFTER SEEDING, IF REQUIRED, ACCORDING TO TEMPORARY
- MULCHING SPECIFICATIONS. (SEE VEGETATIVE COVER SELECTION & MULCHING SPECIFICATION BELOW)
- USE PROPER INOCULAT ON ALL LEGUME SEEDLINGS, USE FOUR (4) TIMES NORMAL RATES WHEN HYDROSEEDING. 7. USE SOD WHERE THERE IS A HEAVY CONCENTRATION OF WATER AND IN CRITICAL
- AREAS WHERE IT IS IMPORTANT TO GET A QUICK VEGETATIVE COVER TO PREVENT EROSION.

MAINTENANCE:

1. TEST FOR SOIL ACIDITY EVERY THREE (3) YEARS AND LIME AS REQUIRED.

EROSION CHECKS

GENERAL:

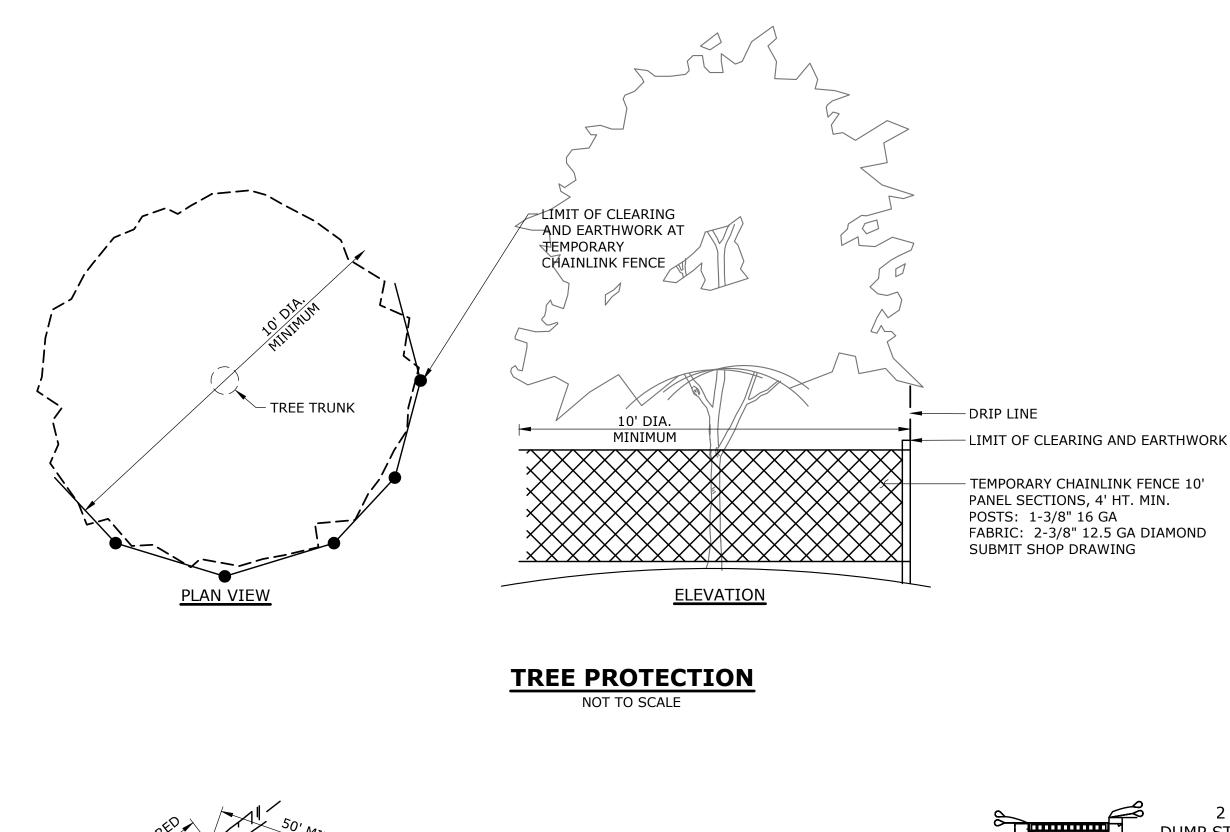
1. TEMPORARY PERVIOUS BARRIERS USING BALES OF HAY OR STRAW, HELD IN PLACE WITH STAKES DRIVEN THROUGH THE BALES AND INTO THE GROUND OR GEOTEXTILE FABRIC FASTENED TO A FENCE POST AND BURIED INTO THE GROUND, SHALL BE INSTALLED AND MAINTAINED AS REQUIRED TO CHECK EROSION AND REDUCE SEDIMENTATION. CONSTRUCTION:

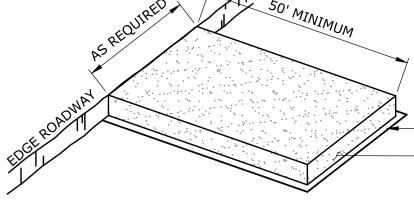
- BALES SHOULD BE PLACED IN A ROW WITH ENDS TIGHTLY ABUTTING THE ADJACENT BALES.
- EACH BALE SHALL BE EMBEDDED INTO THE SOIL A MINIMUM OF FOUR (4") INCHES. BALES SHALL BE SECURELY ANCHORED IN PLACE BY WOOD STAKES OR REINFORCEMENT BARS DRIVEN THROUGH THE BALES AND INTO THE GROUND. THE
- FIRST STAKE IN EACH BALE SHALL BE ANGLED TOWARD THE PREVIOUSLY LAID BALE TO FORCE BALES TOGETHER. 4. GEOTEXTILE FABRIC SHALL BE SECURELY ANCHORED AT THE TOP OF A THREE FOOT (3') HIGH FENCE AND BURIED A MINIMUM OF FOUR INCHES (4") TO THE SOIL. SEAMS BETWEEN SECTIONS OF FILTER FABRIC SHALL OVERLAP A MINIMUM OF TWO FEET (2').

INSTALLATION AND MAINTENANCE:

- BALED HAY EROSION BARRIERS SHALL BE INSTALLED AT ALL STORM SEWER INLETS. BALED HAY EROSION BARRIERS AND GEOTEXTILE FENCE SHALL BE INSTALLED AT
- THE LOCATION INDICATED ON THE PLAN AND IN ADDITIONAL AREAS AS MAY BE DEEMED APPROPRIATE DURING CONSTRUCTION.
- ALL EROSION CHECKS SHALL BE MAINTAINED UNTIL ADJACENT AREAS ARE
- STABILIZED INSPECTION SHALL BE FREQUENT (AT MINIMUM MONTHLY AND BEFORE AND AFTER
- HEAVY RAIN) AND REPAIR OR REPLACEMENT SHALL BE MADE PROMPTLY AS NEEDED. EROSION CHECKS SHALL BE REMOVED WHEN THEY HAVE SERVED THEIR
- USEFULNESS SO AS NOT TO BLOCK OR IMPEDE STORMWATER FLOW OR DRAINAGE.

EROSION CONTROL MAINTENANCE INTERVALS							
EROSION CONTROL MEASURE	CONTROL OBJECTIVE	FAILURE INDICATORS	REMOVAL				
SILT FENCE (SF) (RELATED: IP, STK)	 INTERCEPT, AND REDIRECT/DETAIN SMALL AMOUNTS OF SEDIMENT FROM SMALL DISTURBED AREAS. DECREASE VELOCITY OF SHEET FLOW. PROTECT SENSITIVE SLOPES OR SOILS FROM EXCESSIVE WATER FLOW. 	INSPECT AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL OF 0.5 INCHES OR MORE. ACCUMULATED SEDIMENT MUST BE REMOVED ONCE ITS DEPTH IS EQUAL TO ½ THE TRENCH HEIGHT. INSPECT FREQUENTLY DURING PUMPING OPERATIONS IF USED FOR DEWATERING OPERATIONS.	- PHYSICAL DAMAGE OR DECOMPOSITION - EVIDENCE OF OVERTOPPED OR UNDERCUT FENCE - EVIDENCE OF SIGNIFICANT FLOWS EVADING CAPTURE - REPETITIVE FAILURE	SILT FENCE MAY BE REMOVED AFTER UPHILL AND SENSITIVE AREAS HAVE BEEN PERMANENTLY STABILIZED.			
CONSTRUCTION ENTRANCE (CE)	- REDUCE THE TRACKING OF SEDIMENT OFF-SITE ONTO PAVED SURFACES.	INSPECT AT THE END OF EACH WORK DAY AND IMMEDIATELY REPAIR DAMAGES. PERIODIC ADDITION OF STONE, OR LENGTHENING OF ENTRANCE MAY BE REQUIRED AS CONDITIONS DEMAND. ALL SEDIMENT SPILLED, DROPPED, WASHED, OR TRACKED ONTO PAVED SURFACES AS A RESULT OF INEFFICIENCY OF CONSTRUCTION ENTRANCE SHALL BE IMMEDIATELY REMOVED.	- SEDIMENT IN ROADWAY ADJACENT TO SITE	CONSTRUCTION ENTRANCE MAY BE REMOVED ONCE THE SITE HAS BEEN PERMANENTLY STABILIZED, AND ALL OTHER SECTIONS OF ROADWAY HAVE BEEN PERMANENTLY PAVED.			
INLET PROTECTION (IP)	- PROHIBIT SILT IN CONSTRUCTION-RELATED RUNOFF FROM ENTERING STORM DRAINAGE SYSTEM.	INSPECT AFTER ANY RAIN EVENT. IF FILTER BAG INSIDE CATCH BASIN CONTAINS MORE THAN 6" OF SEDIMENT, REMOVE SEDIMENT FROM BAG. CHECK SURROUNDING SILT FENCE AND HAY BALES PER NOTED ABOVE.	- RIPPED BAG - FAILED HAY BALES / SILT FENCE - SIGNIFICANT SILT PRESENCE IN STORM DRAINAGE SYSTEM OUTFLOW.	INLET PROTECTION MAY BE REMOVED ONCE THE SITE HAS BEEN PERMANENTLY STABILIZED, AND ALL SECTIONS OF ROADWAY HAVE BEEN PERMANENTLY PAVED.			
STOCKPILE PROTECTION (STK)	- RETAIN SOIL STOCKPILE IN LOCATIONS SPECIFIED, AND REDUCE WATER-TRANSPORT.	INSPECT SILT FENCE AT THE END OF EACH WORK DAY AND IMMEDIATELY REPAIR DAMAGES. PERIODIC REINFORCEMENT OF SILT FENCE, OR ADDITION OF HAY BALES MAY BE NECESSARY.	 EVIDENCE OF STOCK PILE DIMINISHING DUE TO RAIN EVENTS FAILURE OF SILT FENCE 	STOCKPILE PROTECTION MAY BE REMOVED ONCE THE STOCKPILE IS USED OR REMOVED.			
TEMPORARY SEDIMENT TRAP (TST)	- DETAIN SEDIMENT-LADEN RUNOFF FROM SMALL DISTURBED AREAS LONG ENOUGH TO ALLOW A MAJORITY OF THE SEDIMENT TO SETTLE OUT.	INSPECT AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL OF 0.5 INCHES OR MORE. STONE OUTLET SHOULD BE AT LEAST 1 FOOT BELOW CREST OF EMBANKMENT. SEDIMENT MUST BE REMOVED WHEN ACCUMULATION REACHES ½ OF THE REQUIRED WET STORAGE.	- TURBID WATER - EXCESSIVE SEDIMENT ACCUMULATION - OVERTOPPING EVIDENCE	TST MAY BE REMOVED ONCE THE CONTRIBUTING DRAINAGE AREA IS PERMANENTLY STABILIZED.			
TEMPORARY DIVERSION BERM/SWALE (DB)	 MINIMIZE VELOCITY AND CONCENTRATION OF SHEET FLOW ACROSS CONSTRUCTION SITE TO A SEDIMENT TRAPPING FACILITY. DIVERT WATER ORIGINATING FROM UNDISTURBED AREA AWAY FROM CONSTRUCTION. 	WHEN LOCATED WITHIN CLOSE PROXIMITY TO ONGOING CONSTRUCTION ACTIVITIES, INSPECT AT THE END OF EACH WORK DAY AND IMMEDIATELY REPAIR DAMAGES. OTHERWISE INSPECT AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL OF 0.5 INCHES OR MORE. REPAIR THE TEMPORARY MEASURE AND ANY OTHER ASSOCIATED MEASURES WITHIN 24 HOURS.	- PHYSICAL DAMAGE - EXCESSIVE SCOURING/EROSION - REPETITIVE FAILURE	TEMPORARY DIVERSIONS MAY BE REMOVED ONCE CONSTRUCTION HAS CEASED AND THE CONTRIBUTING DRAINAGE AREA HAS BEEN PERMANENTLY STABILIZED.			





1. CONSTRUCTION ENTRANCE PAD SHALL BE INSTALLED AND MAINTAINED

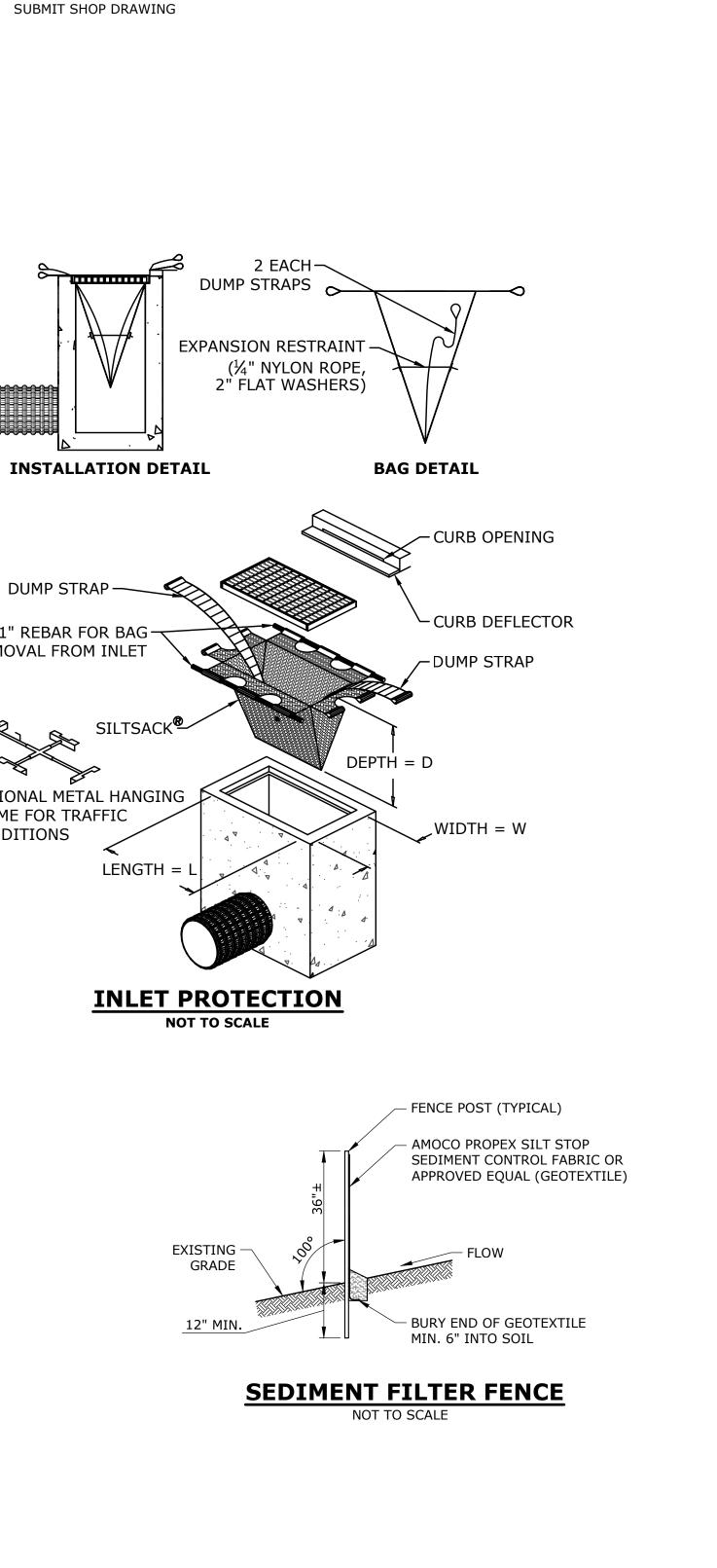
CONSTRUCTION ENTRANCE PAD

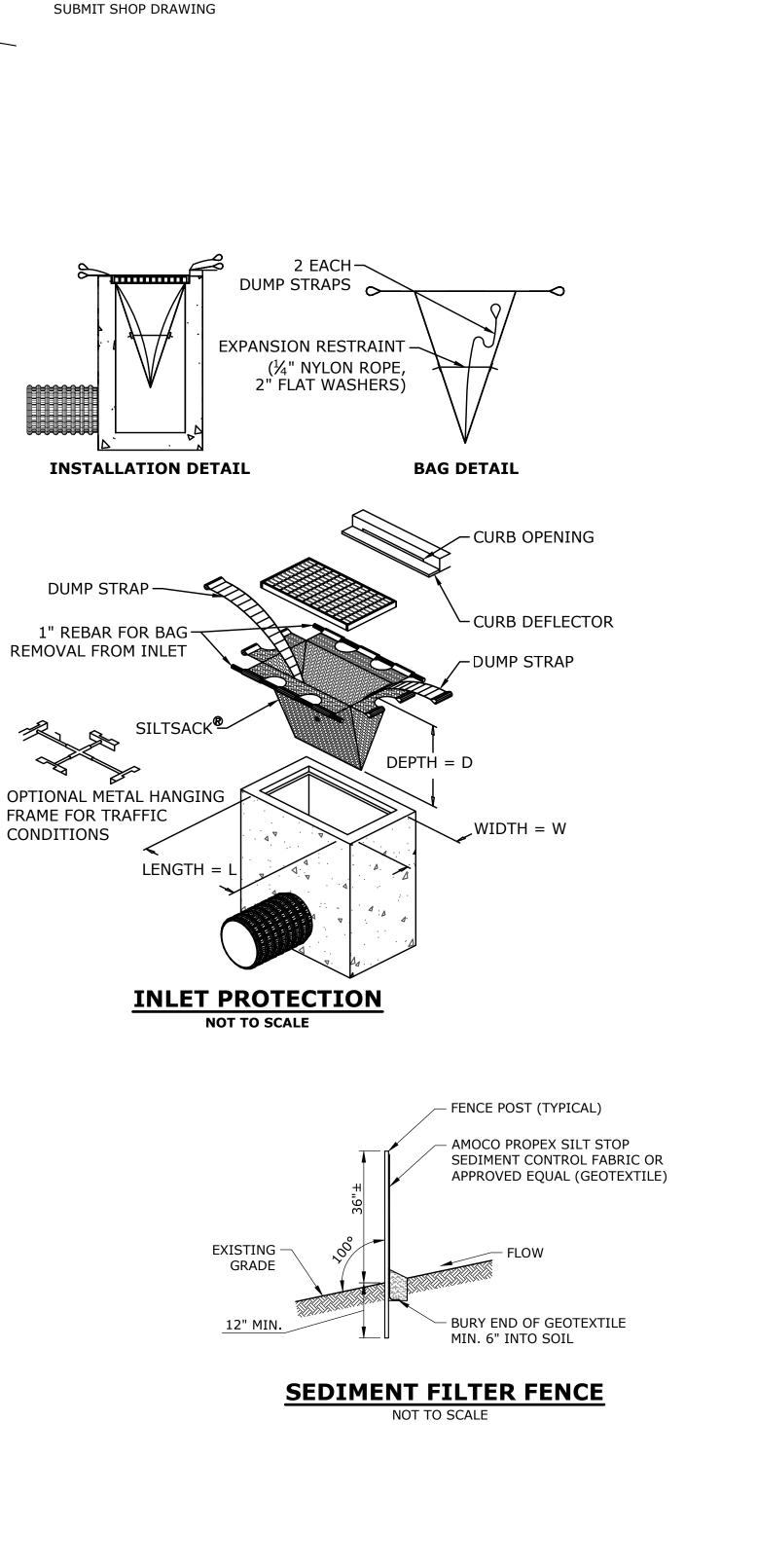
NOT TO SCALE

DURING OPERATIONS WHICH GENERATE VEHICULAR TRACKING OF MUD.

NOTES:

FILTER FABRIC ON COMPACTED SUBGRADE NO 3. (2") BROKEN OR CRUSHED STONE. 6" MINIMUM THICKNESS

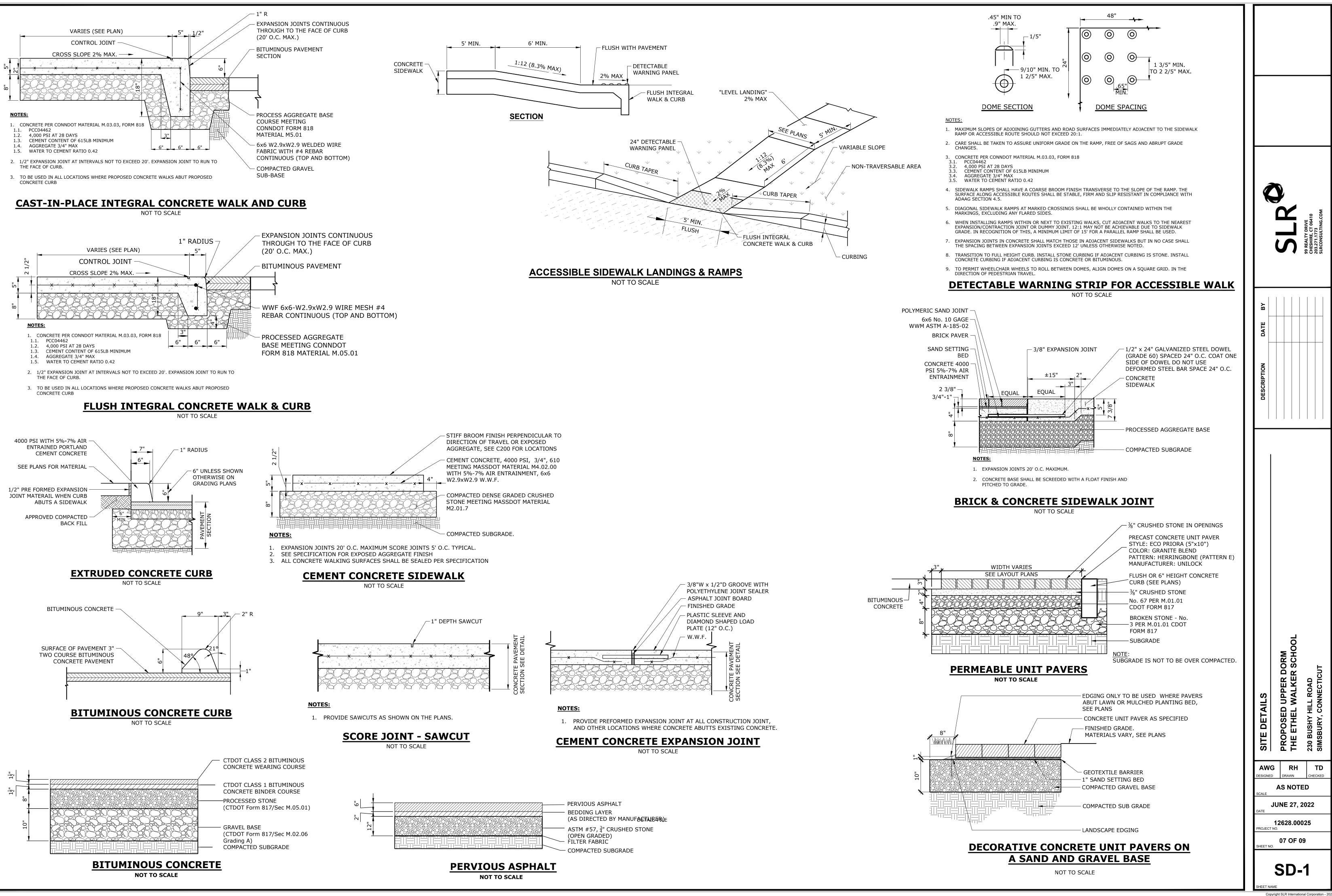


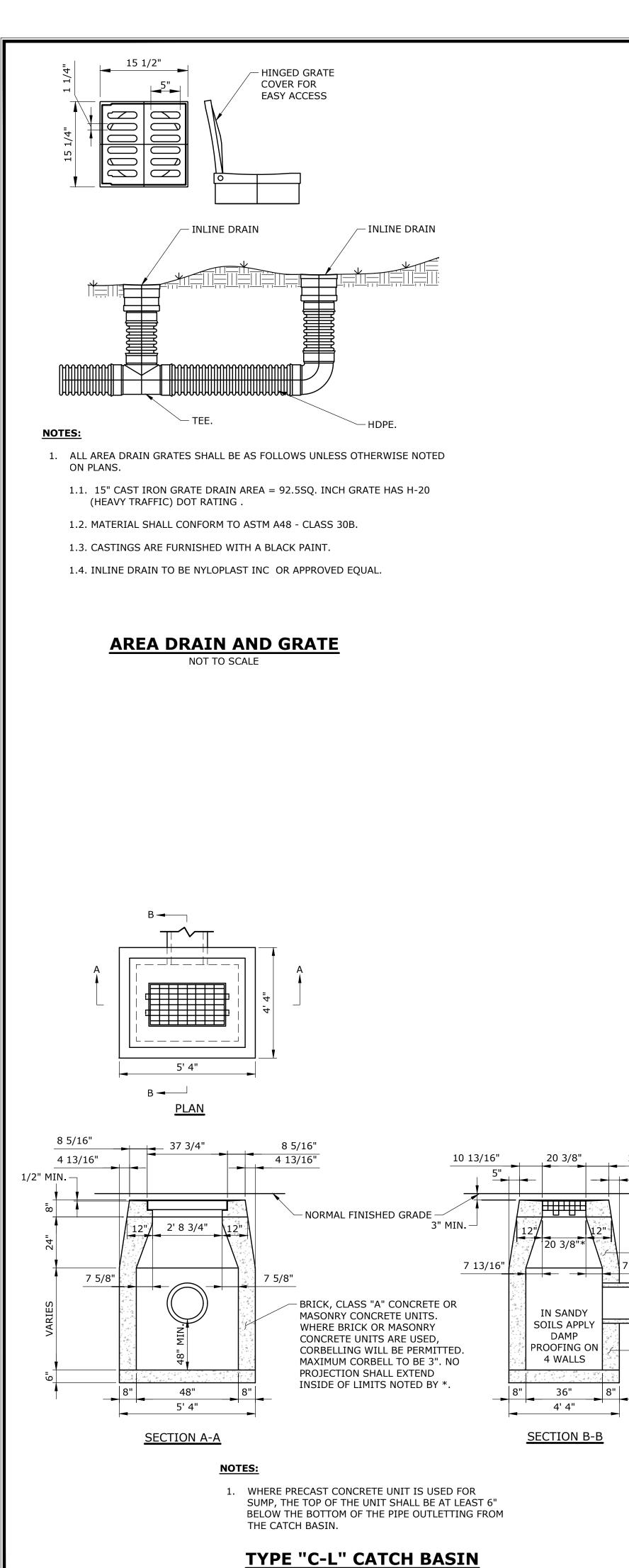


ECI SP S Δ S EROSION PROPOSED UPPER DORM THE ETHEL WALKER SCHO AND Ш SEDIN RH AWG TD **AS NOTED** JUNE 27, 2022 12628.00025 06 OF 09 SE-2

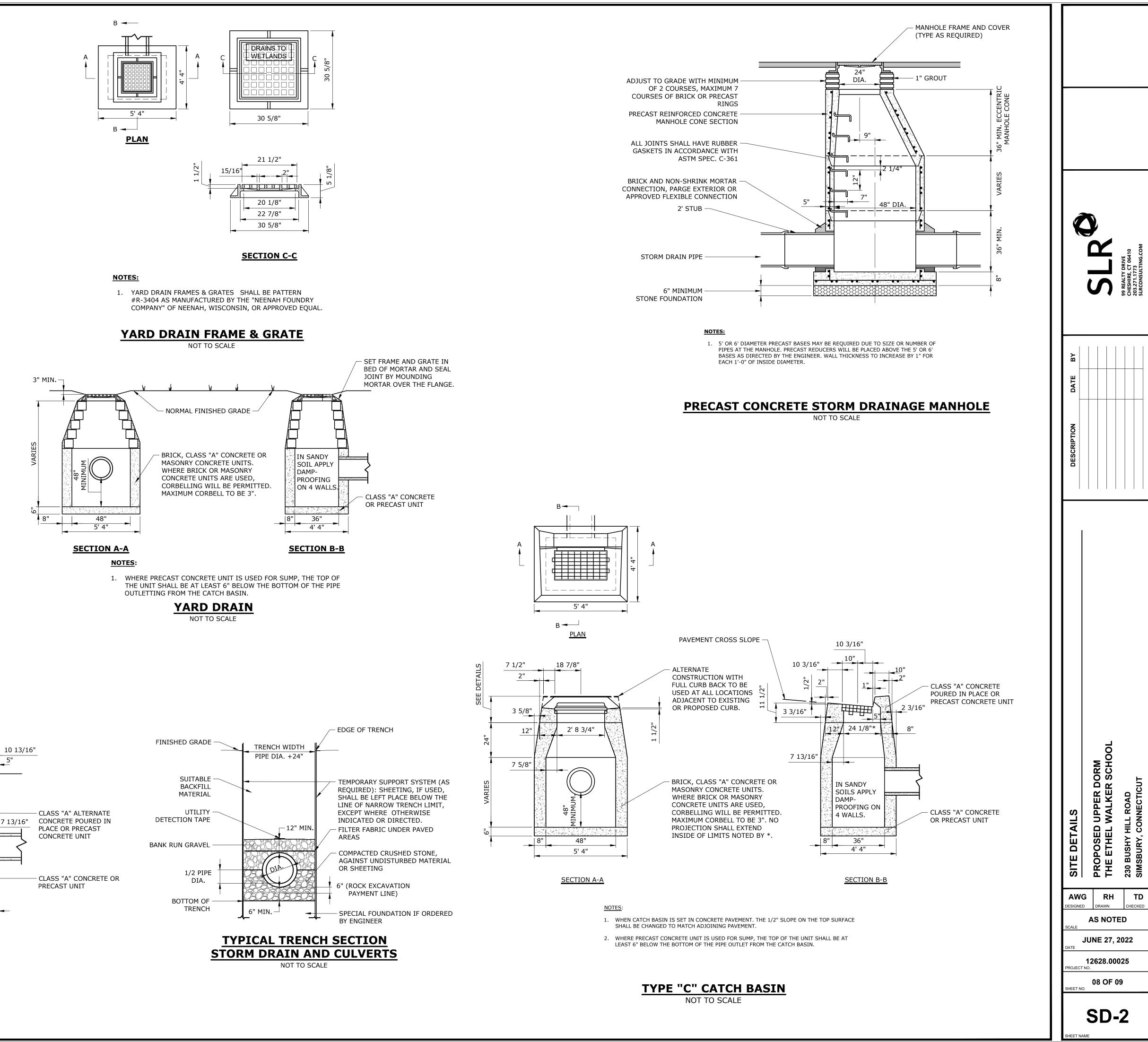
Copyright SLR International Corporation - 2021



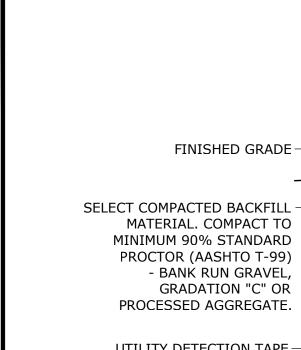




NOT TO SCALE



Copyright SLR International Corporation - 2021



UTILITY DETECTION TAPE -

1/2 PIPE DIAMETER -

BOTTOM OF TRENCH-

GRADATION "C" OR PROCESSED AGGREGATE.

BANK RUN GRAVEL-

6" ROCK EXCAVATION PAYMENT LINE

- COMPACTED CRUSHED STONE, AGAINST UNDISTURBED MATERIAL OR SHEETING

- SURFACE TREATMENT (SEE NOTE 1)

TEMPORARY SUPPORT SYSTEM AS REQUIRED:

TRENCH LIMIT, EXCEPT WHERE OTHERWISE

SHEETING, IF USED, SHALL BE PLACED

BELOW THE LINE OF NARROW

INDICATED OR DIRECTED.

- EDGE OF TRENCH

- SPECIAL FOUNDATION IF ORDERED BY ENGINEER

NOTES:

1. SEE APPROPRIATE DETAIL FOR PAVEMENT REPAIR INFORMATION WHEN INSTALLING SANITARY SEWER MAINS IN PAVED AREAS.

SANITARY SEWER TRENCH

NOT TO SCALE

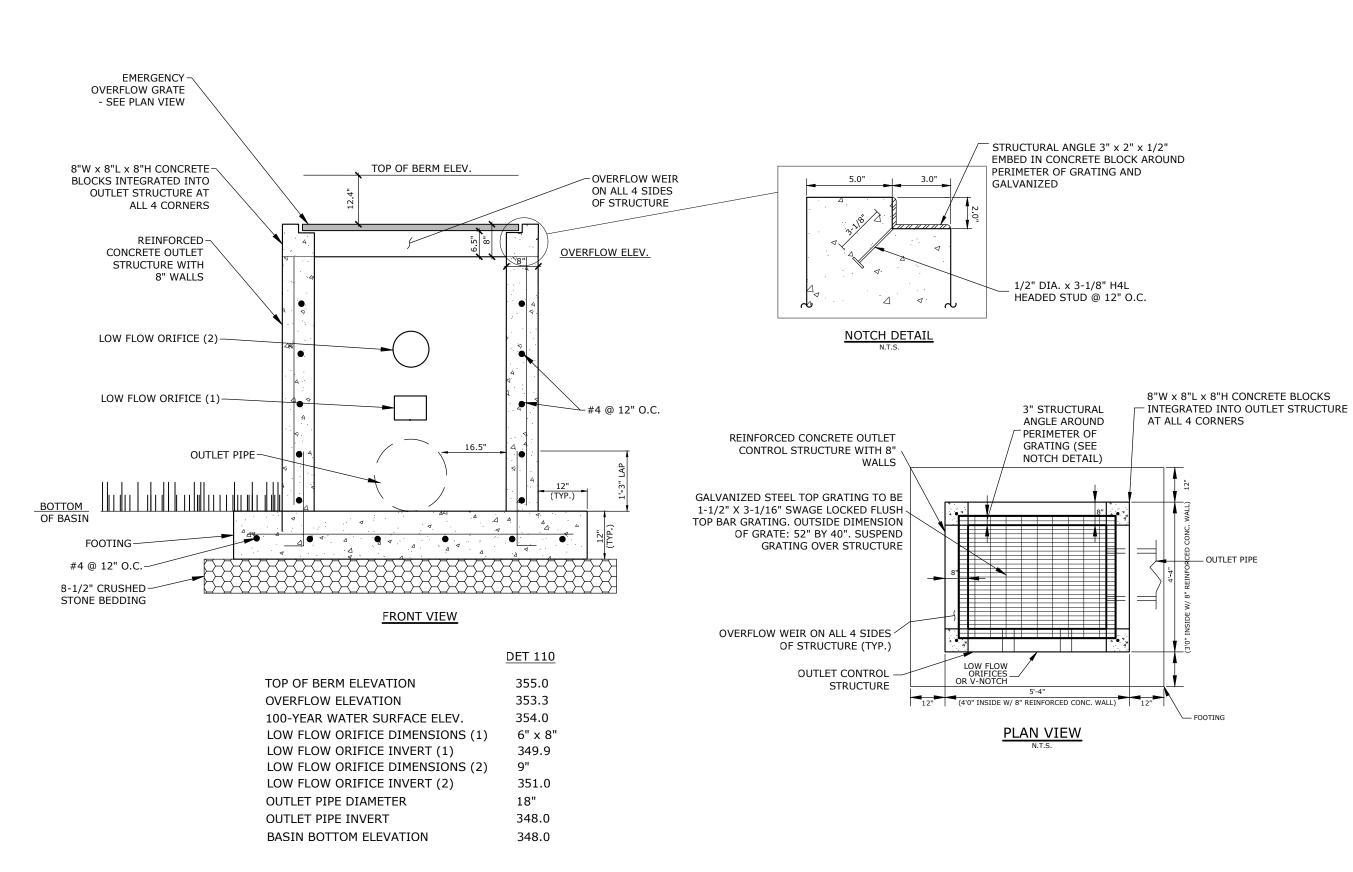
TRENCH WIDTH

<u>-12"</u>

MINIMUM

MINIMUM

PIPE DIAMETER +2

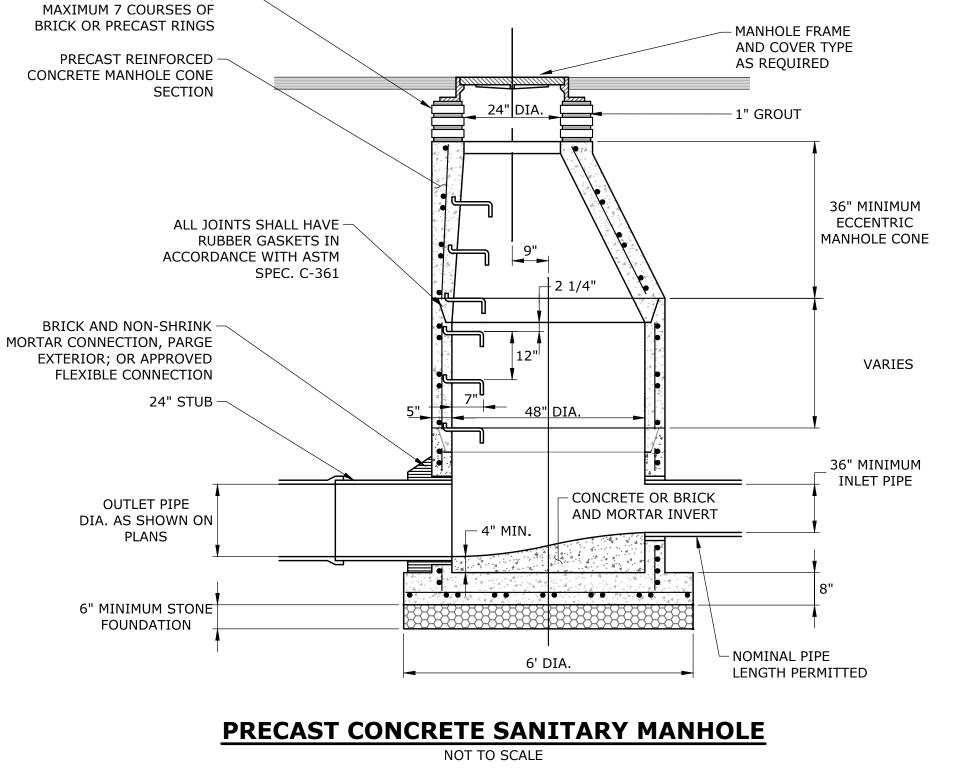


DETENTION BASIN 110 OUTLET CONTROL STRUCTURE SCALE: 1"=2'



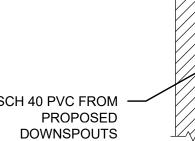


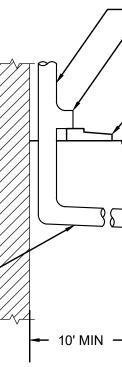
ADJUST TO GRADE WITH -MINIMUM OF 2 COURSES,



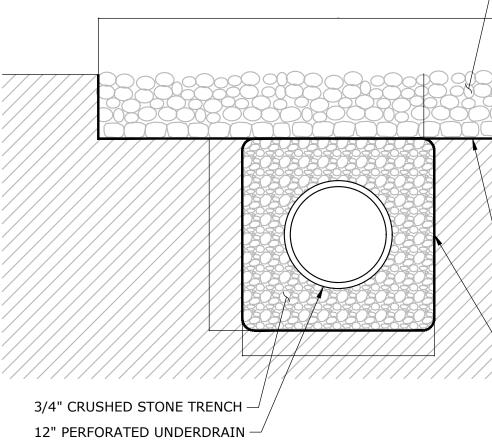


FINISHED GRADE -

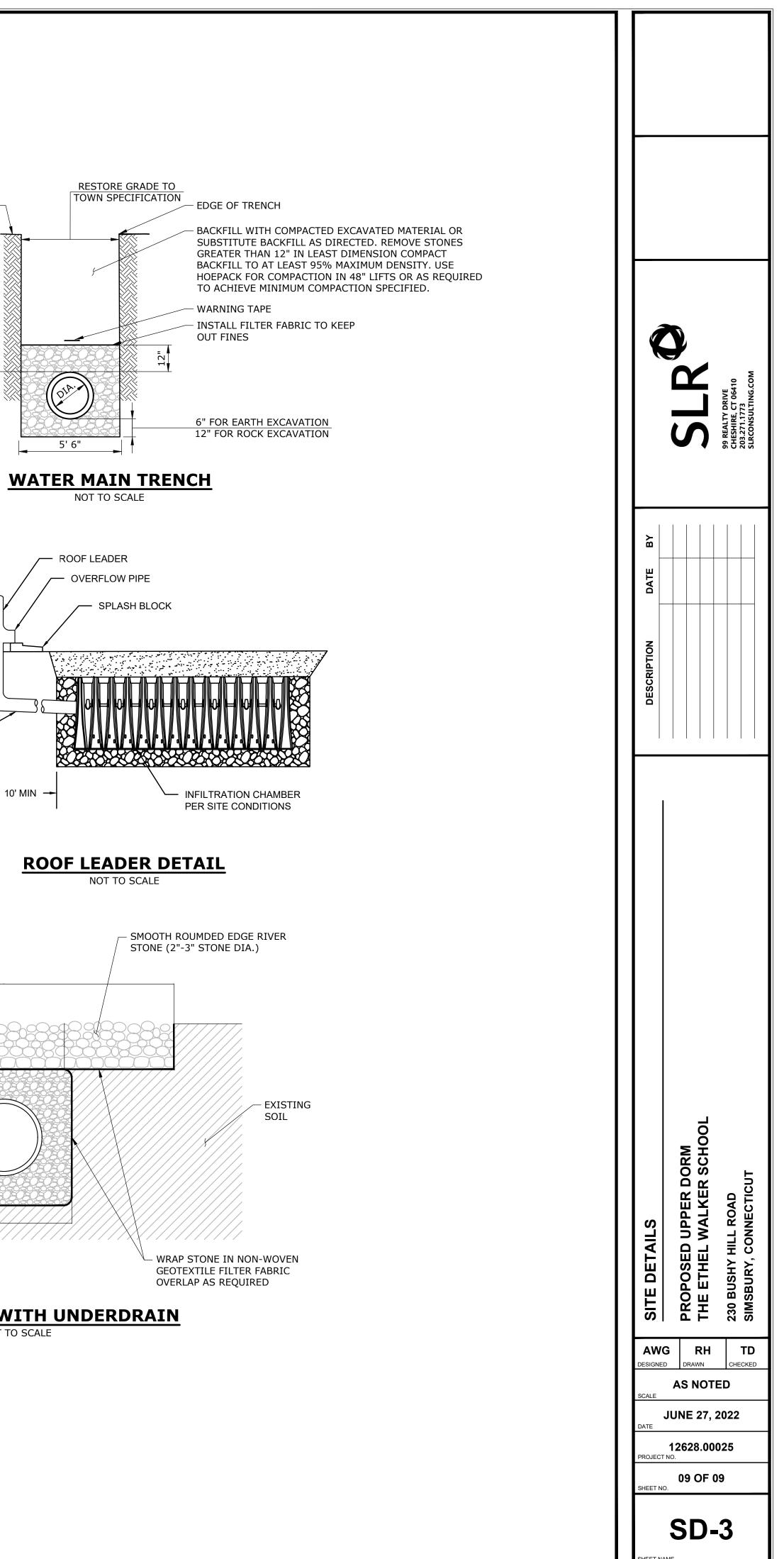


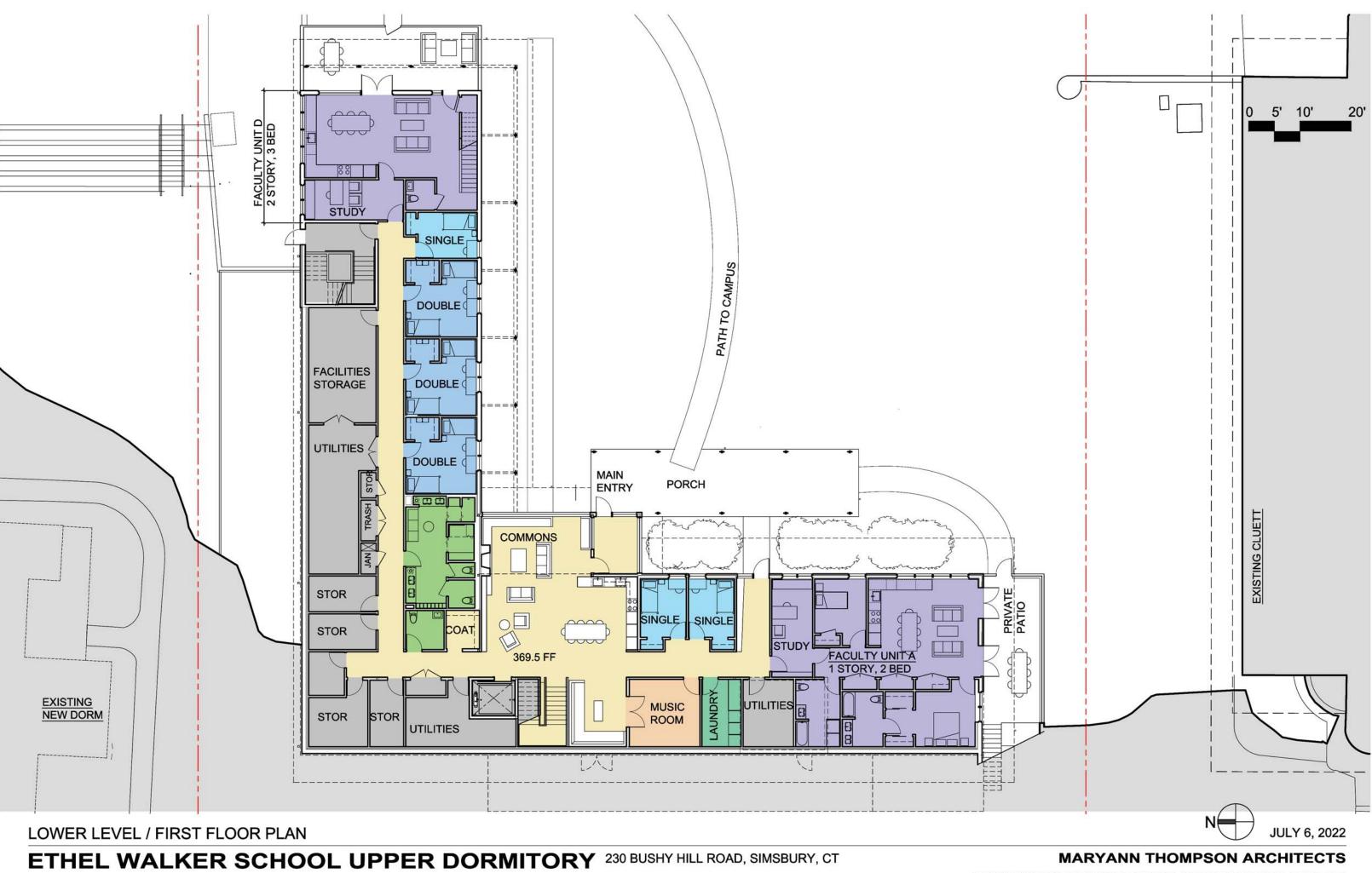


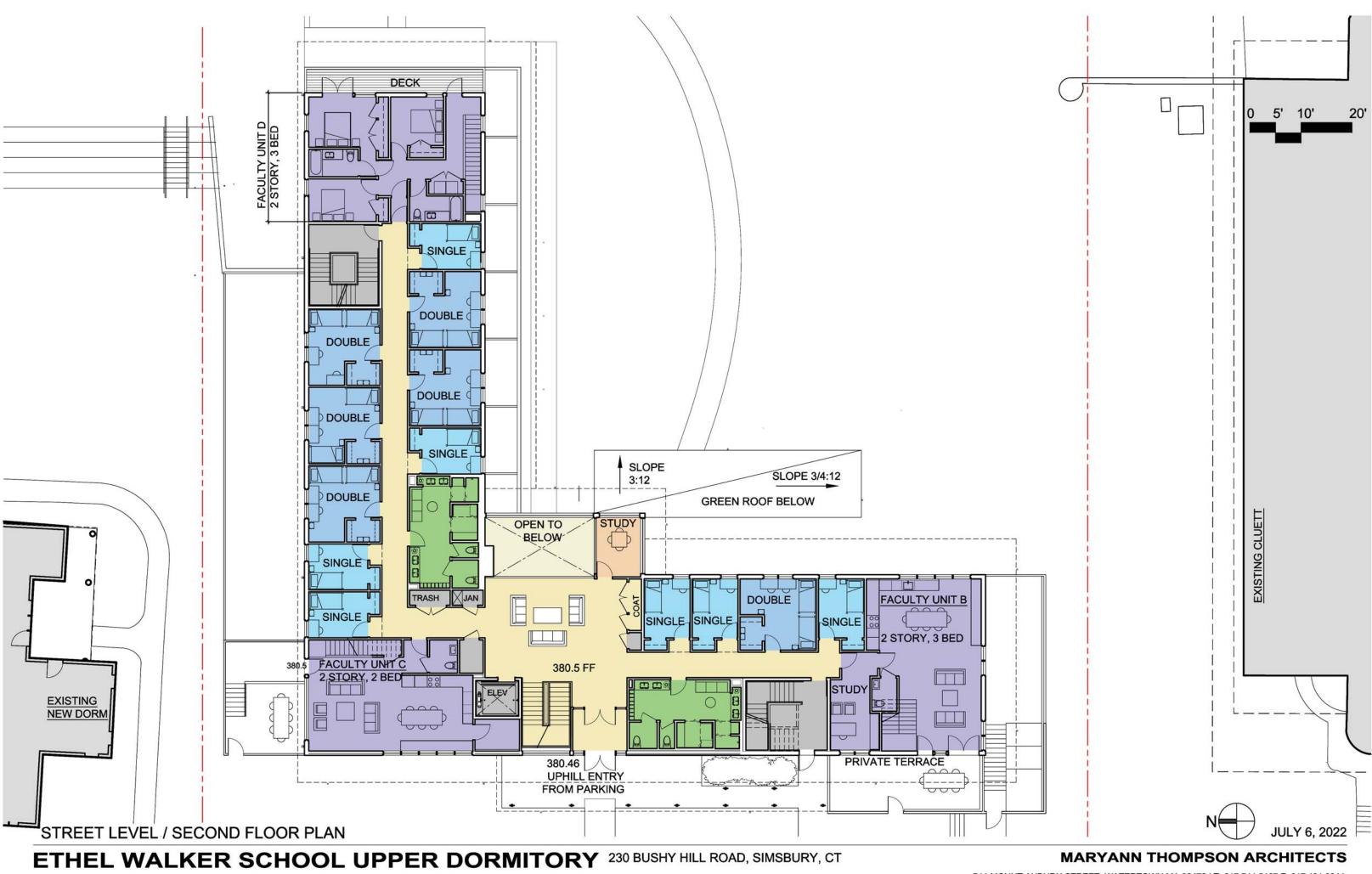
4" SCH 40 PVC FROM



GRAVEL STRIP WITH UNDERDRAIN NOT TO SCALE

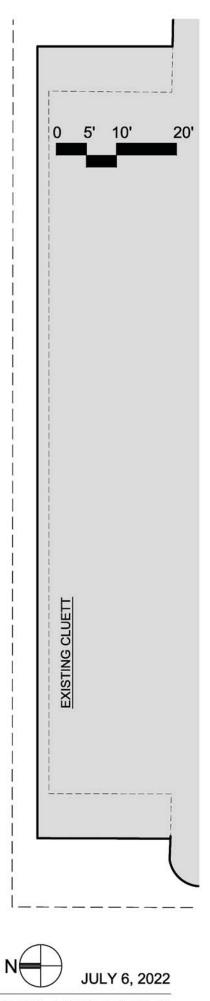






THIRD FLOOR PLAN

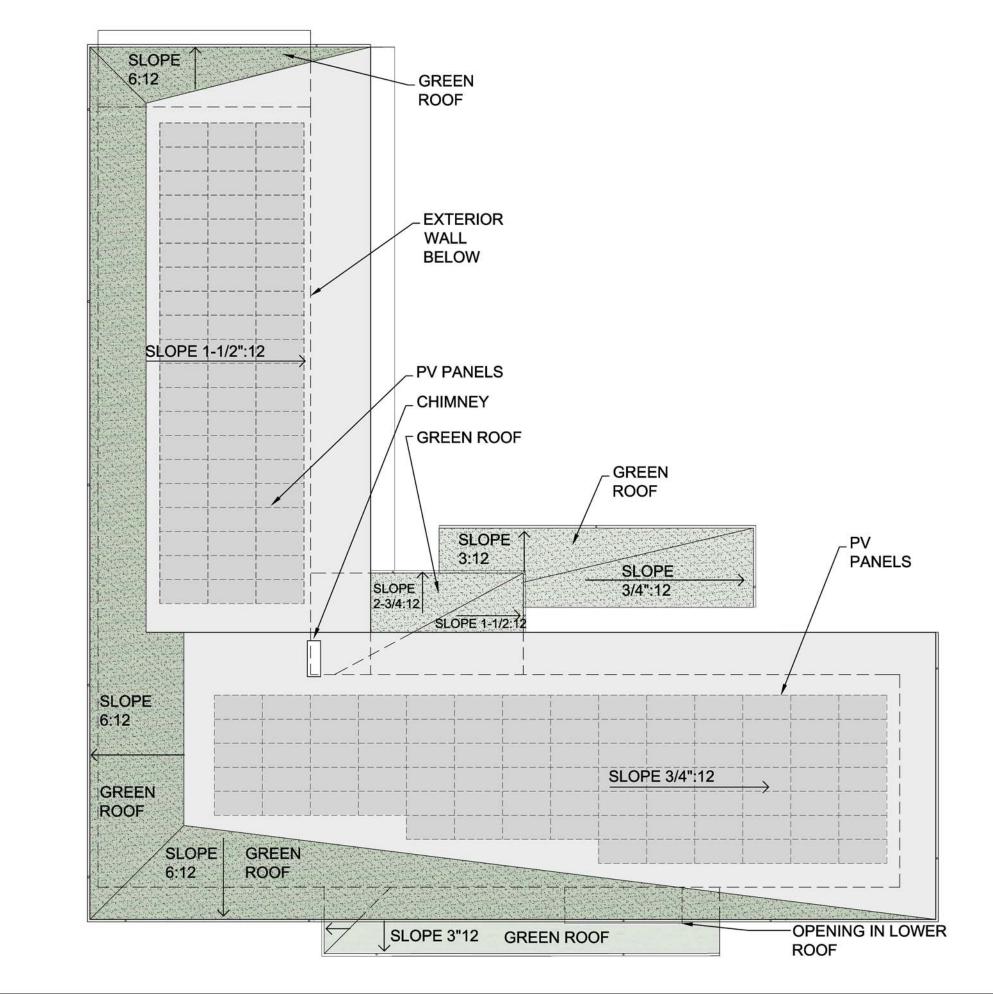


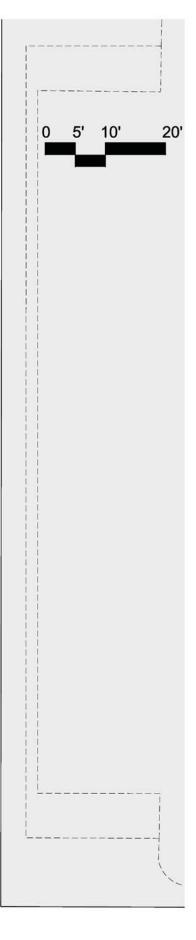


MARYANN THOMPSON ARCHITECTS

ETHEL WALKER SCHOOL UPPER DORMITORY 230 BUSHY HILL ROAD, SIMSBURY, CT

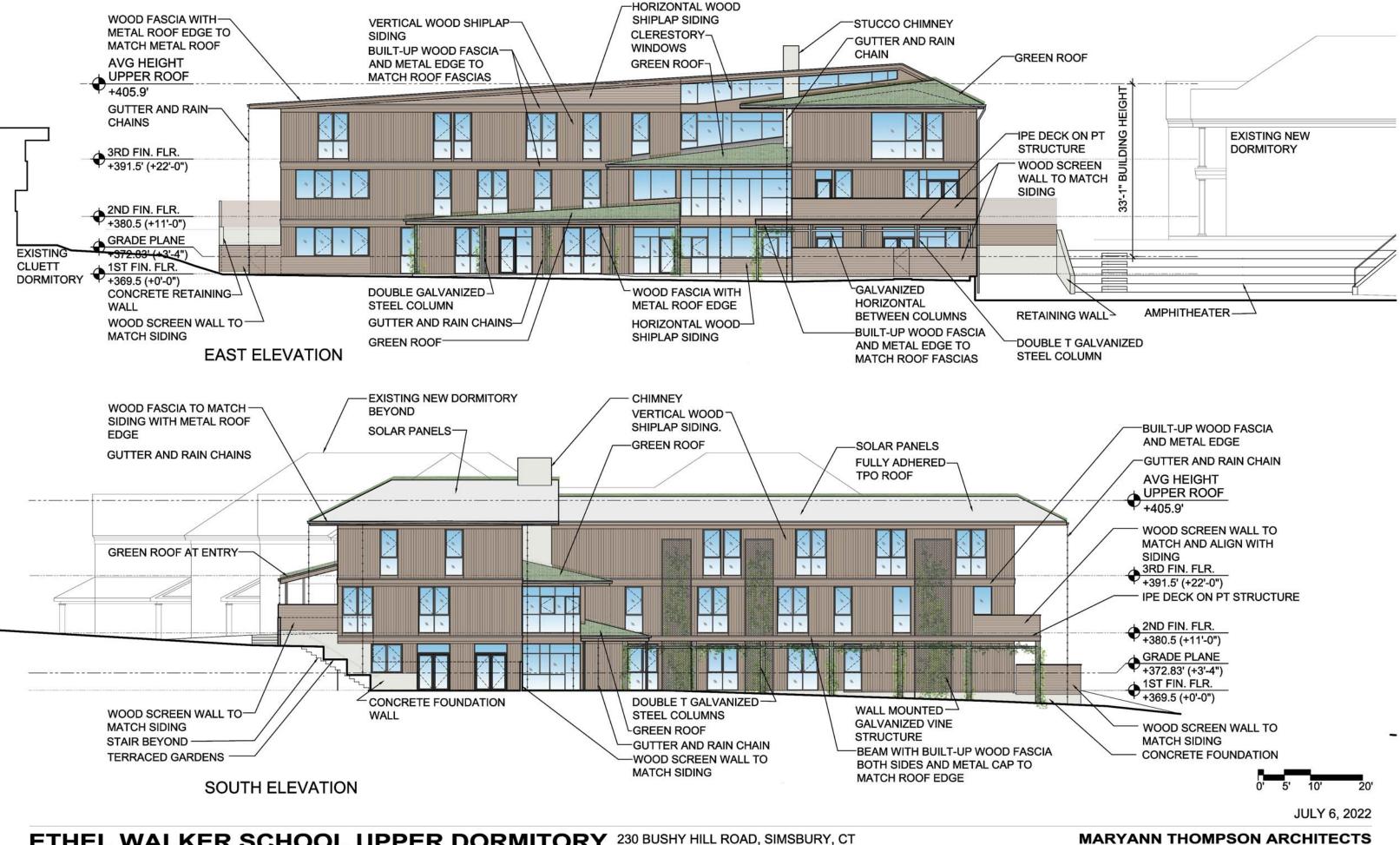
ROOF PLAN



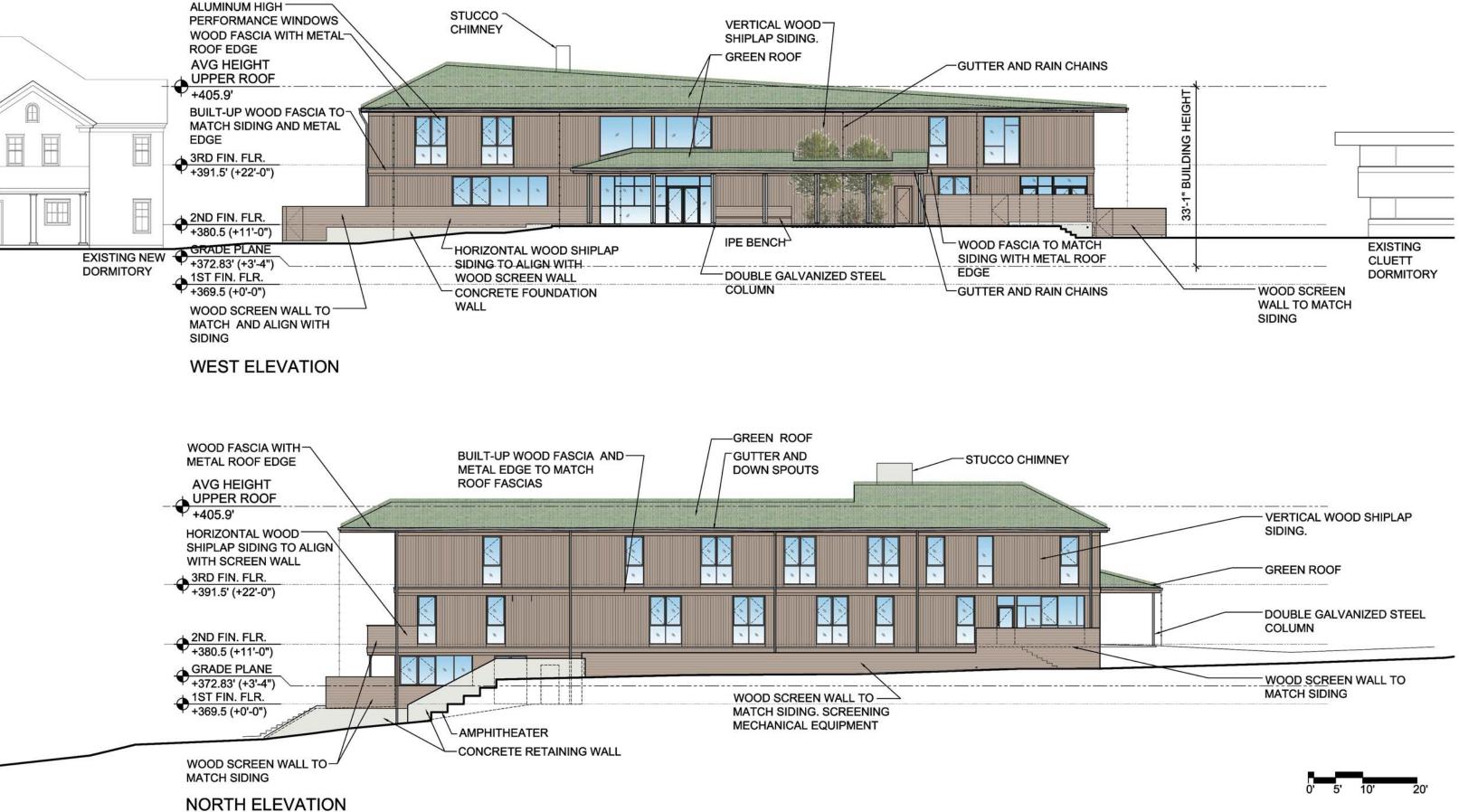




MARYANN THOMPSON ARCHITECTS



ETHEL WALKER SCHOOL UPPER DORMITORY 230 BUSHY HILL ROAD, SIMSBURY, CT



744 MOUNT

JULY 6, 2022

MARYANN THOMPSON ARCHITECTS

ETHEL WALKER SCHOOL UPPER DORM

Drainage Report

Prepared for:

Ethel Walker School

230 Bushy Hill Road

Simsbury, CT 06070

SLR #141.12628.00025.0010

June 27, 2022



Drainage Report

Ethel Walker School Upper Dorm 230 Bushy Hill Road Simsbury, Connecticut June 27, 2022 SLR #141.12628.00025.0010

This Drainage Report has been prepared in support of the proposed dormitory to be constructed at 230 Bushy Hill Road in the town of Simsbury, Connecticut. The development proposes to construct a new dormitory building located between two existing dormitories on the site. New courtyards, sidewalks, and parking areas will be included as well as all associated site infrastructure.



Figure 1 – #D15 115 006 Parcel

Table 1 – Stormwater Data

Parcel Size Total	106.1 acres
Existing Impervious Area (Watershed Area)	1.10 acres
Proposed Impervious Area (Watershed Area)	1.61 acres
Soil Types (Hydrologic Soil Group)	"B" and "C"
Parcel Zoning Code	R-40
Existing Land Use	Woods, open space, bituminous driveway, parking lot, sidewalk, and building
Proposed Land Use	Woods, open space, bituminous driveway, parking lot, sidewalk, and building
Design Storm for Stormwater Management (Town of Simsbury)	No increases in peak rates of runoff for the 2-, 10-, 25-, 50-, and 100-year storms, Connecticut Department of Energy & Environmental Protection (CTDEEP) Water Quality Volume (WQV)
Water Quality Measures	2-foot sump catch basin, retention storage
Design Storm for Storm Drainage (Town of Simsbury)	25-year storm
Federal Emergency Management Agency Special Flood Hazard Areas	Area of Minimal Flood Hazard (Zone X)
Connecticut Department of Energy & Environmental Protection Aquifer Protection Areas	Not Applicable

STORMWATER MANAGEMENT APPROACH

The stormwater management system for this site has been designed utilizing Best Management Practices (BMPs) to provide water quality management and to ensure that predevelopment peak rates of runoff would not be exacerbated due to the new development. The proposed design was planned in accordance with the *Simsbury Stormwater Article* dated September 28, 2011, as included as part of the Town's Land Use Department, and the Connecticut Department of Energy & Environmental (CTDEEP) *2004 Stormwater Manual.*

The performance standards outlined in the *Simsbury Stormwater Article* are organized into the following three areas:

- 1. Planning and Site Design Criteria Checklist
- 2. Stormwater Quantity and Quality Requirements
- 3. Design and Construction Requirements



1. Planning and Site Design Criteria Checklist

The goal is to preserve natural resources, maintain existing drainage patterns to the maximum extent possible, and manage rainfall on the site through a series of BMPs. An improvement in site runoff conditions is expected based on the proposed stormwater improvements planned for the project. The proposed project will expand the existing stormwater treatment train to consist of a catch basin with 2-foot sump and retention storage.

2. Stormwater Quantity and Quality Requirements

2.1 Redevelopment

Projects with more than 50 percent predevelopment impervious surface cover are considered redevelopment projects. At a minimum, redevelopment projects must implement planning, design criteria, and structural BMP measures to meet water quality treatment and recharge volume requirements for at least 50 percent of the postdevelopment effective impervious area.

Based on visual investigation of existing land use, soil subsurface testing, and aerial photogrammetry, the site's land use consists mostly of the existing school building, paved parking lots and drives, sidewalks, grassed areas, and some woods.

Types of Impervious Areas	Area (acres)
Buildings	0.28
Paved	0.79
Gravel	0.03
Total Impervious Area	1.10
Project Limits	4.51
% Impervious =	24.3%

Table 2 Existing Impervious Area Chart

Per the definition of impervious area in the Simsbury Zoning Regulations, the existing land use was delineated. The project limits were determined to contain approximately 24.3 percent of impervious area. Therefore, the adjustment factor of 50 percent was not applied to the water quality standard requirements.

2.2 Peak Rate

The postdevelopment impervious area will be increased compared to the predevelopment conditions' impervious coverage. The proposed development will expand the existing detention basin that is designed to mitigate the increase in stormwater runoff from the site due to the new impervious surfaces. Therefore, the peak-rate requirements from the *Simsbury Stormwater Article* for the 2-, 10-, 25-, 50-, and 100-year, 24-hour design storm events are met. A detailed hydrologic analysis has been prepared, and the results of the peak rates of runoff are included in that section of this report.



2.3 Recharge Volume

The required recharge volume was calculated by multiplying the Effective Impervious Area – Volume (EIA-V) by the groundwater recharge depth. The EIA-V is the effective impervious area after the application of any Site BMP volume incentives.

The site is predominantly located within Hydrologic Soil Groups "B" and "C." Therefore, the groundwater recharge depth used in the computations was 0.35 as a conservative calculation, per Table 1.2 of the *Simsbury Stormwater Article*.

The required Recharge Volume was calculated to be 0.016 acre-feet (ac-ft). The provided volume achieved by the proposed stormwater basin is 0.144 ac-ft, thus meeting Simsbury's Recharge Volume requirements. The volume provided is also used toward meeting the CTDEEP Water Quality Volume (WQV) and Simsbury Groundwater Recharge Volume (GRV) requirements, which are further discussed in this report.

2.4 Water Quality

The required water quality volume for the project is 1 inch of rainfall over the Effective Impervious Area – Water Quality (EIA-WQ).

The stormwater basin has approximately 0.144 ac-ft of storage volume below the lower orifice elevation. Therefore, the volume provided meets Simsbury's WQV requirements. The underground storage chambers will each include an isolator row and will be preceded by a pretreatment proprietary hydrodynamic separator. These units were sized based on CTDEEP requirements for Water Quality Flow (WQF), which is discussed in the Water Quality Management section of this report.

2.5 Conveyance

The proposed storm drainage system was designed to provide adequate capacity to convey the 25-year storm event. The discharge capacity of the outlet pipe from the stormwater basin was sized to provide adequate capacity for the 100-year storm event.

The computer program titled *Hydraflow Storm Sewers Extension for AutoCAD® Civil 3D® 2019* by Autodesk, Inc., Version 2018.3, was used for designing the proposed storm drainage collection system. Storm drainage computations performed include pipe capacity and hydraulic grade line calculations. The contributing watershed to each individual catch basin inlet was delineated to determine the drainage area and land coverage. These values were used to determine the stormwater runoff to each inlet using the Rational Method. The rainfall intensities for the site were obtained from the National Oceanic and Atmospheric Administration (NOAA) Atlas 14, Volume 10, Precipitation Frequency Data Server (PFDS).



2.6 Offsite Mitigation and Stormwater Mitigation Bank

Offsite mitigation and stormwater mitigation bank are not applicable to this project.

2.7 Site BMP Incentive Credits

Site BMP Incentive Credits allow for a reduction in the postdevelopment impervious area used for calculation purposes, resulting in the Effective Impervious Area (EIA). The project site does not take credit for any of the Site BMP Incentives listed in the *Simsbury Stormwater Article*.

3. Design and Construction Requirements

3.1 BMP Requirements

The development has been designed in accordance with the guidelines of the CTDEEP 2004 Stormwater Quality Manual. All construction and erosion and sediment controls provided are in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. Structural stormwater BMPs were selected using the guidance of the Site BMP Selection Matrix (Table 1.3) of the Simsbury Stormwater Article.

3.2 Special Detention Areas

Special Detention Areas are not applicable to the proposed project.

STORMWATER OPERATION AND MAINTENANCE

A detailed Stormwater Management Operation and Maintenance Plan is included in the proposed Utilities Plan Sheet UT, which comprises of recommended frequency of services, procedures for inspection and maintenance of the proposed BMPs, disposal of materials, and owner's responsibilities.

WATER QUALITY MANAGEMENT

In addition to the water quality requirements from the Town of Simsbury, the proposed drainage plan has also been developed following the recommendations set forth in the CTDEEP *2004 Stormwater Quality Manual.* All of the treatment measures described in this section will help maintain water quality of the stormwater runoff from the proposed site.

Stormwater runoff from the proposed improvements will be collected by a subsurface pipe and catch basin drainage system. The proposed drainage system will include catch basins with 2-foot sumps that will trap sediments.

The volume requirements associated with the CTDEEP WQV and GRV were achieved by the retention volume provided in the stormwater detention basin. The CTDEEP *2004 Stormwater Quality Manual* (Chapter 7) recommends methods for sizing stormwater treatment measures with WQV and GRV



computations. The WQV addresses the initial stormwater runoff also commonly referred to as the "first flush" runoff. The WQV provides adequate volume to store the initial 1 inch of runoff, which tends to contain the highest concentrations of potential pollutants. The GRV provides adequate volume to maintain the predevelopment annual groundwater recharge and promote infiltration based on the soils found on the site. When provided, the GRV will achieve similar stormwater infiltration capabilities and maintain adequate groundwater recharge. All supporting calculations for the volume provided as well as WQV and GRV computations have been included in the Appendix of this report.

HYDROLOGIC ANALYSIS

A detailed hydrologic analysis has been conducted to analyze the predevelopment and postdevelopment peak-flow rates from the site. One analysis point was chosen based on the fact that it receives stormwater runoff from the total proposed project site, including the contributing offsite upstream areas. The existing subwatershed and existing detention basin design was used to determine runoff for current site conditions. The existing watershed was then modified to reflect the proposed changes to the site and analyze the hydrology under proposed conditions. The total watershed area delineated is approximately 4.51 acres under existing conditions and 4.74 acres proposed conditions. A watershed map for both existing and proposed conditions is included in the Appendix of this report. The following table provides a brief description of the analysis point used in this hydrology study:

Analysis Point	Description
А	Outflow from Detention Basin

The method of predicting the surface water runoff rates utilized in this analysis is a computer program titled *Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2019* by Autodesk, Inc., Version 2020. The *Hydrographs* program is a computer model that utilizes the methodologies set forth in the *Technical Release No. 55* (TR-55) manual and *Technical Release No. 20* (TR-20) computer model, originally developed by the United States Department of Agriculture – Natural Resources Conservation Service (USDA-NRCS). The *Hydrographs* computer modeling program is primarily used for conducting hydrology studies such as this one.

The *Hydrographs* computer program forecasts the rate of surface water runoff based upon several factors. The input data includes information on land use, hydrologic soil type, vegetation, contributing watershed area, time of concentration, rainfall data, storage volumes, and the hydraulic capacity of structures. The computer model predicts the amount of runoff as a function of time, with the ability to include the attenuation effect due to dams, lakes, large wetlands, floodplains, and stormwater management basins. The input data for rainfalls with statistical recurrence frequencies of 2, 10, 25, 50, and 100 years was obtained from the NOAA Atlas 14, Volume 10 database.

Storm Frequency	Rainfall (inches)
2-year	3.37
10-year	5.43
25-year	6.72
50-year	7.66
100-year	8.71

Table 4 NOAA Rainfall Amounts

Land use for the site under existing and proposed conditions was determined from field survey, town topographic maps, and aerial photogrammetry. Land use types used in the analysis included woods, grassed or open space, building, and impervious (drives, sidewalks, parking). Soil types in the watershed were determined from the CTDEEP Geographic Information System (GIS) database of the USDA-NRCS soil survey for Hartford County, Connecticut. For the analysis, the site was determined to contain hydrologic soil types "B" and "C" as classified by NRCS. Composite runoff Curve Number (CN) for each subwatershed was calculated based on the different land use and soil types. The time of concentration (Tc) was estimated for each subwatershed using the TR-55 methodology and was computed by summing all travel times through the watershed as sheet flow, shallow concentrated flow, and channel flow.

The existing conditions were modeled with the *Hydrographs* program to determine the peak-flow rates for the various storm events at the analysis point. A revised model was developed incorporating the proposed grading, storm drainage, proposed land coverage, and the expanded stormwater detention basin. The flows obtained with the revised model were then compared to the results of the existing conditions model. A reduction in the predevelopment peak runoff rates is expected under proposed conditions due to the proposed improvements to the site. The following peak rates of runoff were obtained from the *Hydrographs* hydrology results:

Analysis Point A – Outflow from Detention Basin					
	Peak Runoff Rate (cubic feet per second)				
Storm Frequency (years)	2	10	25	50	100
Existing Conditions	2.7	10.1	14.7	17.2	21.0
Proposed Conditions	2.7	5.5	12.1	16.6	19.1

Detention Basin 110					
	Water Surface Elevation (feet)				
Storm Frequency (years)	2 10 25 50 100				
Existing Conditions*	352.2	353.2	353.4	353.6	353.8
Proposed Conditions**	351.5	353.1	353.6	353.7	354.0

*Top Elevation of Berm = 354.7 feet

**Top Elevation of Berm = 355.0 feet

CONCLUSION

The results of the hydrologic analysis demonstrate that there will be no increases in peak-flow rates from the project site. The proposed project will introduce a new stormwater treatment train consisting of catch basins with 2-foot sumps and retention storage.

The proposed stormwater management design was planned in accordance with the Town of Simsbury Stormwater regulations and the CTDEEP *2004 Stormwater Manual.* The design meets Simsbury's stormwater requirements for redevelopment, peak rate, recharge volume, water quality, and conveyance.

All supporting documentation and stormwater-related computations are attached to this report along with the *Hydraflow Hydrographs* model results for stormwater management and *Hydraflow Storm Sewers* model results for the proposed storm drainage system. Illustrative watershed maps for both existing and proposed conditions are also attached to this report.

Attachments

Appendix A – United States Geological Survey Location Map Appendix B – Federal Emergency Management Agency Flood Insurance Rate Map Appendix C – Natural Resources Conservation Service Hydrologic Soil Group Map Appendix D – Storm Drainage Computations Appendix E – Water Quality Computations Appendix F – Hydrologic Analysis – Input Computations Appendix G – Hydrologic Analysis – Computer Model Results Appendix H – Watershed Maps

12628.00025.jn1522.rpt.docx



APPENDIX A

UNITED STATES GEOLOGICAL SURVEY LOCATION MAP

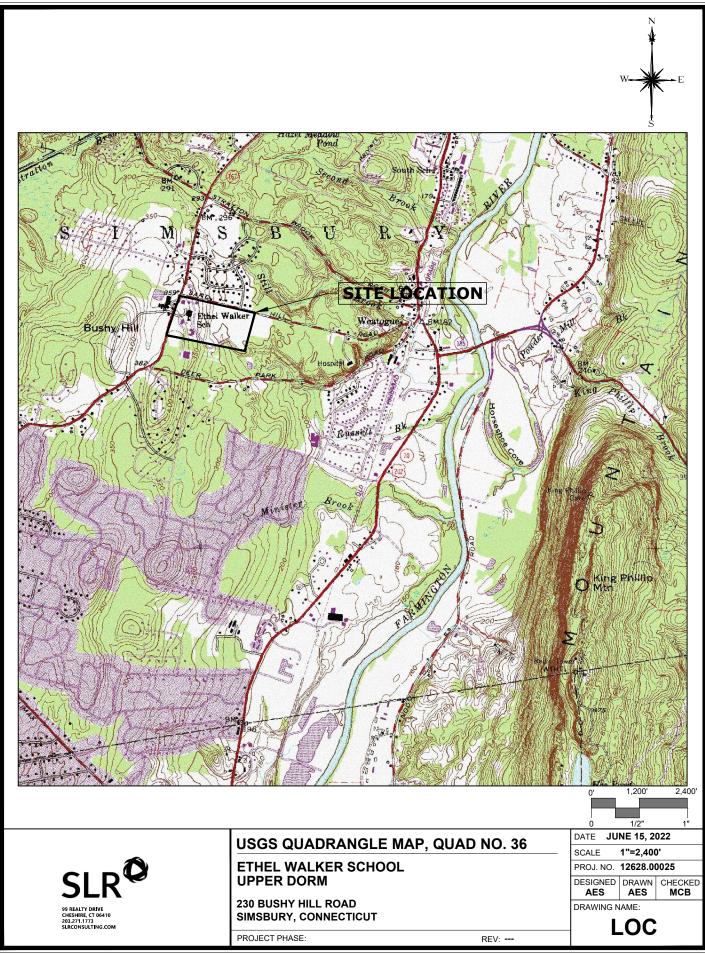
Drainage Report

Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

June 27, 2022



Copyright SLR Consulting, Inc - 2022



APPENDIX B

FEDERAL EMERGENCY MANAGEMENT AGENCY FLOOD INSURANCE RATE MAP

Drainage Report

Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

June 27, 2022

National Flood Hazard Layer FIRMette



Legend

72°50'18"W 41°51'8"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation AREA OF MINIMAL FLOOD HAZARD Town of Simsbury **Coastal Transect** Zce X Mase Flood Elevation Line (BFE) 090035 Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** ----OTHER Profile Baseline 09003C0327F FEATURES Hydrographic Feature eff. 9/26/2008 **Digital Data Available** No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards Zone A The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/9/2022 at 2:46 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 72°49'40"W 41°50'41"N Feet 1:6.000 unmapped and unmodernized areas cannot be used for

250

500

1.500

1,000

2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

regulatory purposes.



APPENDIX C

NATURAL RESOURCES CONSERVATION SERVICE HYDROLOGIC SOIL GROUP MAP

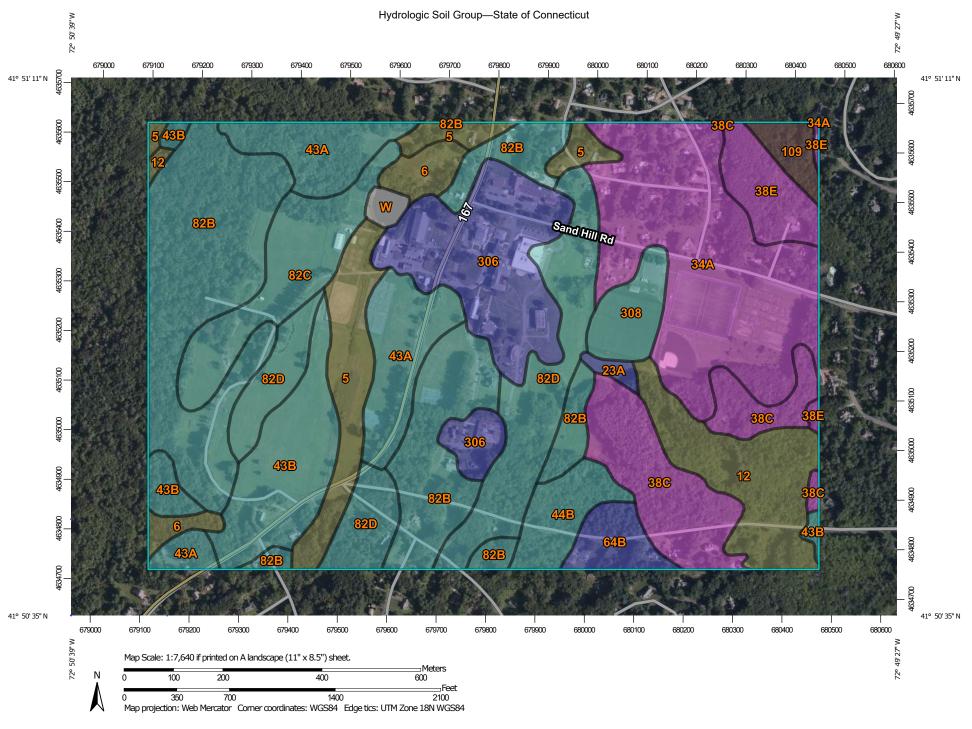
Drainage Report

Ethel Walker School

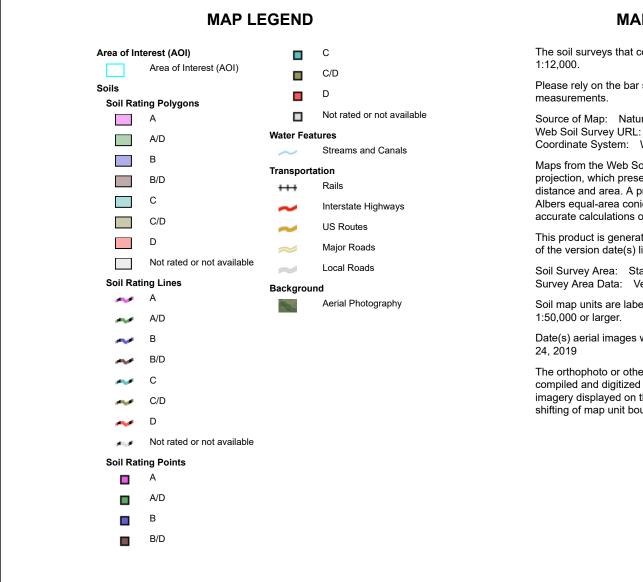
230 Bushy Hill Road

Simsbury, Connecticut 06070

June 27, 2022



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at

Please rely on the bar scale on each map sheet for map

Source of Map: Natural Resources Conservation Service Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut Survey Area Data: Version 21, Sep 7, 2021

Soil map units are labeled (as space allows) for map scales

Date(s) aerial images were photographed: Aug 24, 2019-Oct

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI	
5	Wilbraham silt loam, 0 to 3 percent slopes	C/D	16.4	5.4%	
6	Wilbraham and Menlo soils, 0 to 8 percent slopes, extremely stony	C/D	5.1	1.7%	
12	Raypol silt loam	C/D	17.0	5.6%	
23A	Sudbury sandy loam, 0 to 5 percent slopes	В	1.1	0.3%	
34A	Merrimac fine sandy loam, 0 to 3 percent slopes	A	41.8	13.8%	
38C	Hinckley loamy sand, 3 to 15 percent slopes	A	20.3	6.7%	
38E	Hinckley loamy sand, 15 to 45 percent slopes	A	7.9	2.6%	
43A	Rainbow silt loam, 0 to 3 percent slopes	С	21.4	7.0%	
43B	Rainbow silt loam, 3 to 8 percent slopes	С	19.2	6.3%	
44B	Rainbow silt loam, 2 to 8 percent slopes, very stony	С	6.8	2.2%	
64B	Cheshire fine sandy loam, 3 to 8 percent slopes, very stony	В	5.0	1.6%	
82B	Broadbrook silt loam, 3 to 8 percent slopes	С	59.3	19.5%	
82C	Broadbrook silt loam, 8 to 15 percent slopes	С	15.2	5.0%	
82D	Broadbrook silt loam, 15 to 25 percent slopes	С	30.0	9.9%	
109	Fluvaquents-Udifluvents complex, frequently flooded	B/D	3.1	1.0%	
306	Udorthents-Urban land complex	В	26.8	8.8%	
308	Udorthents, smoothed	С	6.1	2.0%	
W	Water		1.3	0.4%	
Totals for Area of Inter	rest	1	303.7	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



APPENDIX D

STORM DRAINAGE COMPUTATIONS

Drainage Report

Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

June 27, 2022

Project: <u>Proposed Upper Dorm</u> Location: <u>Simsbury</u> , Connecticut			By: <u>AES</u> Checked:		Date: <u>6/7/22</u> Date:		
Basin Name	Impervious Area C=0.9 (sf)	Grassed Area C=0.3 (sf)	Wooded Area C=0.2 (sf)	Total Area (sf)	Total Area (ac)	Weighted C	Tc (min
			System 100				
AD 7	318	51	0	369	0.01	0.82	5.0
CLCB 10	6038	2958	3440	12436	0.29	0.56	5.0
AD 11	2914	1518	1802	6234	0.14	0.55	5.0
AD 14	2496	586	2202	5284	0.12	0.54	5.0
AD 15	942	224	1540	2706	0.06	0.45	5.0
AD 12	2283	2493	1401	6177	0.14	0.50	5.0
YD 3	0	90	0	90	0.01	0.30	5.0
AD 4	1209	2623	3471	7303	0.17	0.35	18.5
AD 5	0	405	0	405	0.01	0.30	5.0
Q TO MH 9	5559	7837	7925	21321	0.49	0.42	5.0

-	ect: <u>Proposed Upper D</u> on: <u>Simsbury, Connec</u>			Check	By: <u>AES</u> ed:	Dat	e: <u>6/7/22</u> e:
	Total Roof F	Runoff to Propo	sed Storm D	rainage Syste	em (In Hydraflow	Model)	
	KKNOWN Q TO	ROOF TO YD					
	MH 9	3					
С	0.42	0.90					
	9.06	9.06					
А	0.49	0.28					
Q	1.86	2.28					



Precipitation Frequency Data Server



NOAA Atlas 14, Volume 10, Version 3 Location name: Simsbury, Connecticut, USA* Latitude: 41.8484°, Longitude: -72.833° Elevation: 345.08 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-	based poi	nt precipi [.]	tation freq	luency est	timates v	vith 90%	confiden	ce interv	als (in in	ches) ¹
Duration				Average i	recurrence	interval (y	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.351 (0.270-0.451)	0.420 (0.323-0.541)	0.533 (0.408-0.688)	0.626 (0.477-0.814)	0.755 (0.558-1.03)	0.852 (0.618-1.19)	0.953 (0.673-1.38)	1.07 (0.715-1.59)	1.23 (0.793-1.89)	1.36 (0.858-2.14)
10-min	0.497 (0.382-0.639)	0.595 (0.457-0.766)	0.755 (0.578-0.976)	0.887 (0.676-1.15)	1.07 (0.791-1.46)	1.21 (0.875-1.68)	1.35 (0.953-1.96)	1.51 (1.01-2.25)	1.74 (1.13-2.69)	1.92 (1.22-3.03)
15-min	0.585 (0.450-0.752)	0.700 (0.538-0.901)	0.888 (0.680-1.15)	1.04 (0.795-1.36)	1.26 (0.930-1.71)	1.42 (1.03-1.98)	1.59 (1.12-2.30)	1.78 (1.19-2.64)	2.04 (1.32-3.16)	2.26 (1.43-3.57)
30-min	0.791 (0.609-1.02)	0.949 (0.730-1.22)	1.21 (0.925-1.56)	1.42 (1.08-1.85)	1.72 (1.27-2.34)	1.94 (1.41-2.70)	2.17 (1.53-3.15)	2.43 (1.63-3.61)	2.79 (1.81-4.32)	3.09 (1.96-4.88)
60-min	0.998 (0.768-1.28)	1.20 (0.921-1.54)	1.53 (1.17-1.97)	1.80 (1.37-2.34)	2.17 (1.61-2.96)	2.46 (1.78-3.43)	2.75 (1.94-3.99)	3.08 (2.07-4.58)	3.54 (2.29-5.48)	3.92 (2.48-6.19)
2-hr	1.29 (0.997-1.65)	1.54 (1.19-1.97)	1.96 (1.51-2.51)	2.30 (1.77-2.98)	2.78 (2.07-3.77)	3.13 (2.29-4.36)	3.51 (2.50-5.10)	3.95 (2.66-5.86)	4.61 (3.00-7.11)	5.17 (3.28-8.14)
3-hr	1.48 (1.15-1.89)	1.78 (1.38-2.27)	2.26 (1.75-2.90)	2.67 (2.05-3.43)	3.22 (2.41-4.37)	3.63 (2.67-5.05)	4.07 (2.93-5.93)	4.61 (3.11-6.81)	5.42 (3.53-8.33)	6.12 (3.90-9.61)
6-hr	1.87 (1.46-2.36)	2.26 (1.77-2.86)	2.91 (2.27-3.70)	3.44 (2.67-4.41)	4.18 (3.15-5.65)	4.72 (3.50-6.56)	5.32 (3.86-7.74)	6.06 (4.10-8.92)	7.22 (4.71-11.0)	8.22 (5.25-12.8)
12-hr	2.30 (1.81-2.88)	2.83 (2.23-3.56)	3.70 (2.90-4.67)	4.42 (3.45-5.62)	5.41 (4.11-7.29)	6.14 (4.59-8.51)	6.95 (5.08-10.1)	7.97 (5.41-11.7)	9.57 (6.26-14.6)	11.0 (7.03-17.1)
24-hr	2.68 (2.13-3.35)	3.37 (2.67-4.21)	4.50 (3.55-5.64)	5.43 (4.27-6.86)	6.72 (5.14-9.03)	7.66 (5.77-10.6)	8.71 (6.43-12.7)	10.1 (6.86-14.7)	12.3 (8.05-18.6)	14.2 (9.13-22.0)
2-day	3.01 (2.40-3.73)	3.85 (3.07-4.78)	5.23 (4.16-6.51)	6.37 (5.04-7.99)	7.94 (6.13-10.6)	9.08 (6.90-12.6)	10.4 (7.75-15.2)	12.1 (8.29-17.6)	15.0 (9.89-22.7)	17.7 (11.4-27.2)
3-day	3.28 (2.63-4.04)	4.20 (3.37-5.20)	5.72 (4.57-7.10)	6.98 (5.54-8.72)	8.71 (6.75-11.7)	9.96 (7.61-13.7)	11.4 (8.55-16.6)	13.3 (9.14-19.3)	16.6 (10.9-25.0)	19.6 (12.6-30.1)
4-day	3.52 (2.84-4.34)	4.51 (3.63-5.57)	6.14 (4.91-7.59)	7.48 (5.96-9.32)	9.33 (7.25-12.4)	10.7 (8.16-14.7)	12.2 (9.17-17.8)	14.3 (9.79-20.6)	17.8 (11.7-26.7)	20.9 (13.5-32.2)
7-day	4.22 (3.41-5.16)	5.33 (4.31-6.54)	7.16 (5.77-8.81)	8.67 (6.94-10.7)	10.8 (8.40-14.3)	12.3 (9.42-16.8)	14.0 (10.5-20.2)	16.3 (11.2-23.5)	20.1 (13.3-30.2)	23.6 (15.3-36.1)
10-day	4.91 (3.99-5.98)	6.08 (4.94-7.43)	8.01 (6.48-9.82)	9.61 (7.72-11.9)	11.8 (9.24-15.6)	13.4 (10.3-18.2)	15.2 (11.4-21.8)	17.6 (12.2-25.3)	21.6 (14.3-32.2)	25.1 (16.3-38.3)
20-day	7.08 (5.79-8.57)	8.30 (6.78-10.1)	10.3 (8.39-12.6)	12.0 (9.68-14.7)	14.3 (11.2-18.5)	15.9 (12.3-21.3)	17.8 (13.3-25.1)	20.2 (14.0-28.7)	23.9 (16.0-35.5)	27.2 (17.7-41.4)
30-day	8.90 (7.31-10.7)	10.1 (8.32-12.3)	12.2 (9.95-14.8)	13.9 (11.3-16.9)	16.2 (12.7-20.8)	17.9 (13.8-23.7)	19.7 (14.7-27.4)	22.0 (15.4-31.2)	25.4 (17.0-37.6)	28.4 (18.5-43.0)
45-day	11.2 (9.21-13.4)	12.4 (10.2-15.0)	14.5 (11.9-17.5)	16.3 (13.3-19.8)	18.6 (14.7-23.8)	20.4 (15.7-26.7)	22.3 (16.5-30.4)	24.4 (17.1-34.4)	27.3 (18.3-40.3)	29.7 (19.4-44.9)
60-day	13.0 (10.8-15.6)	14.4 (11.9-17.2)	16.5 (13.6-19.9)	18.3 (15.0-22.2)	20.8 (16.4-26.4)	22.7 (17.4-29.5)	24.6 (18.2-33.2)	26.5 (18.7-37.3)	29.0 (19.5-42.6)	30.9 (20.2-46.6)

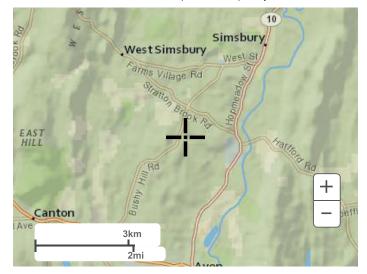
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

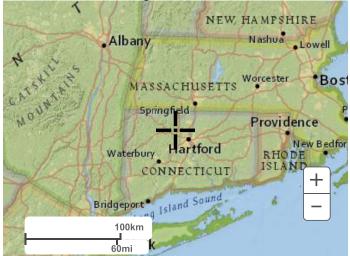
Back to Top

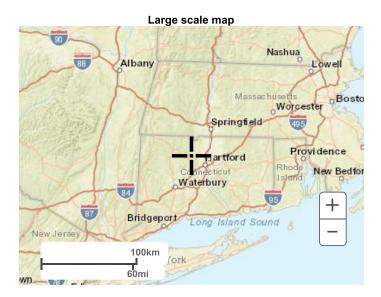
PF graphical

Precipitation Frequency Data Server



Large scale terrain





Large scale aerial

Storm Sewer IDF Curves

Int. (in/hr) 14.00 -- 14.00 100-Yr 12.00 -- 12.00 50-Yr 10.00 -- 10.00 25-Yr 8.00 8.00 10-Yr 6.00 6.00 5-Yr - 4.00 4.00 2-Yr 2.00 -- 2.00 1-Yr 0.00 -- 0.00 0 5 10 15 20 25 30 35 40 45 50 55 60 Time (min)

Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Jun 13 2022

٦

12-inch HDPE @ 0.5%

Circular	
Diameter	(ft)

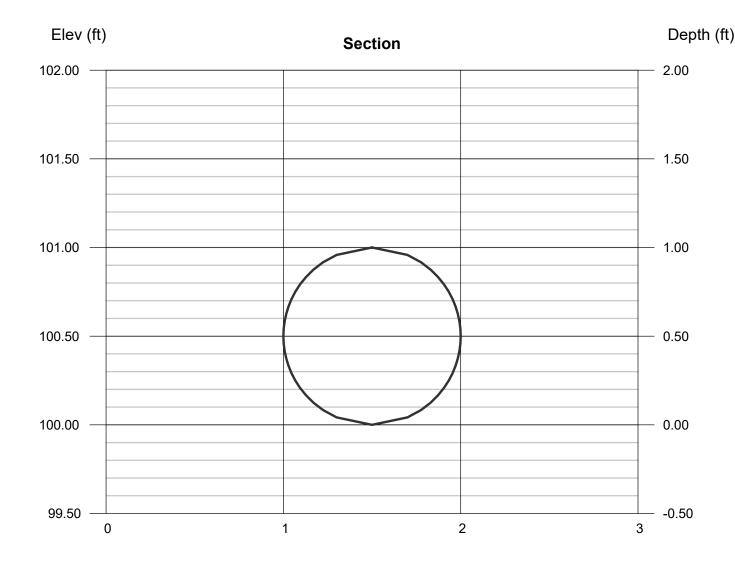
Diameter (ft)	= 1.00
Invert Elev (ft)	= 100.00
Slope (%)	= 0.50
N-Value	= 0.012

Calculations

Q vs Depth Compute by: No. Increments = 10

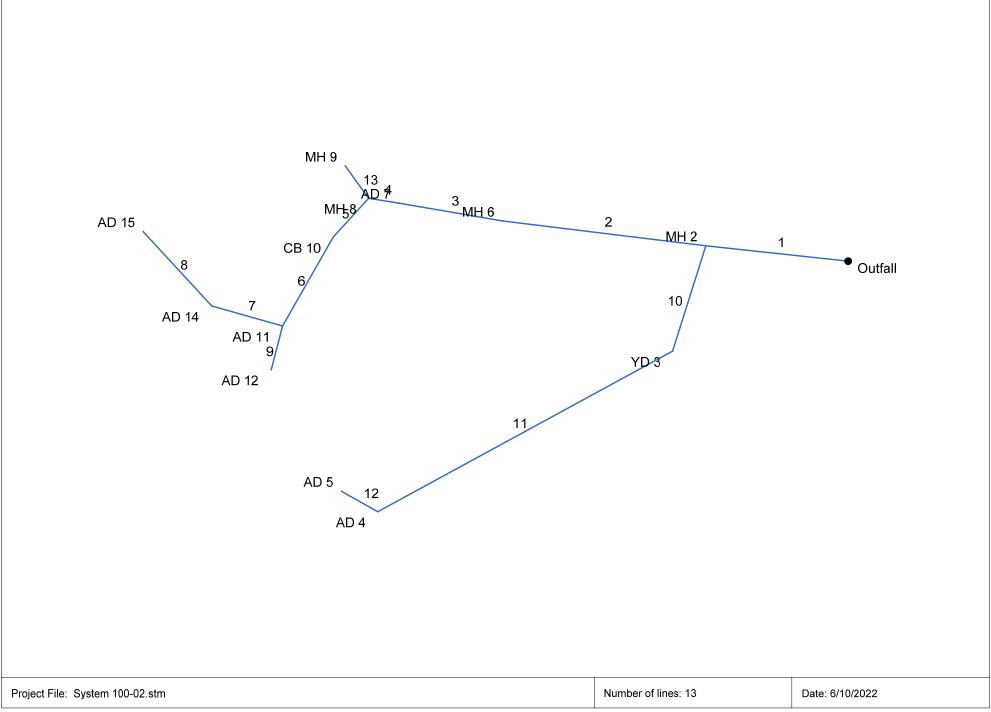
Highlighted		
Depth (ft)	=	1.00
Q (cfs)	=	2.728
Area (sqft)	=	0.79
Velocity (ft/s)	=	3.47
Wetted Perim (ft)	=	3.14
Crit Depth, Yc (ft)	=	0.71
Top Width (ft)	=	0.00
EGL (ft)	=	1.19

Q > ROOF TO YD 3 = 2.28 cfs



Reach (ft)

Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Storm Sewer Inventory Report

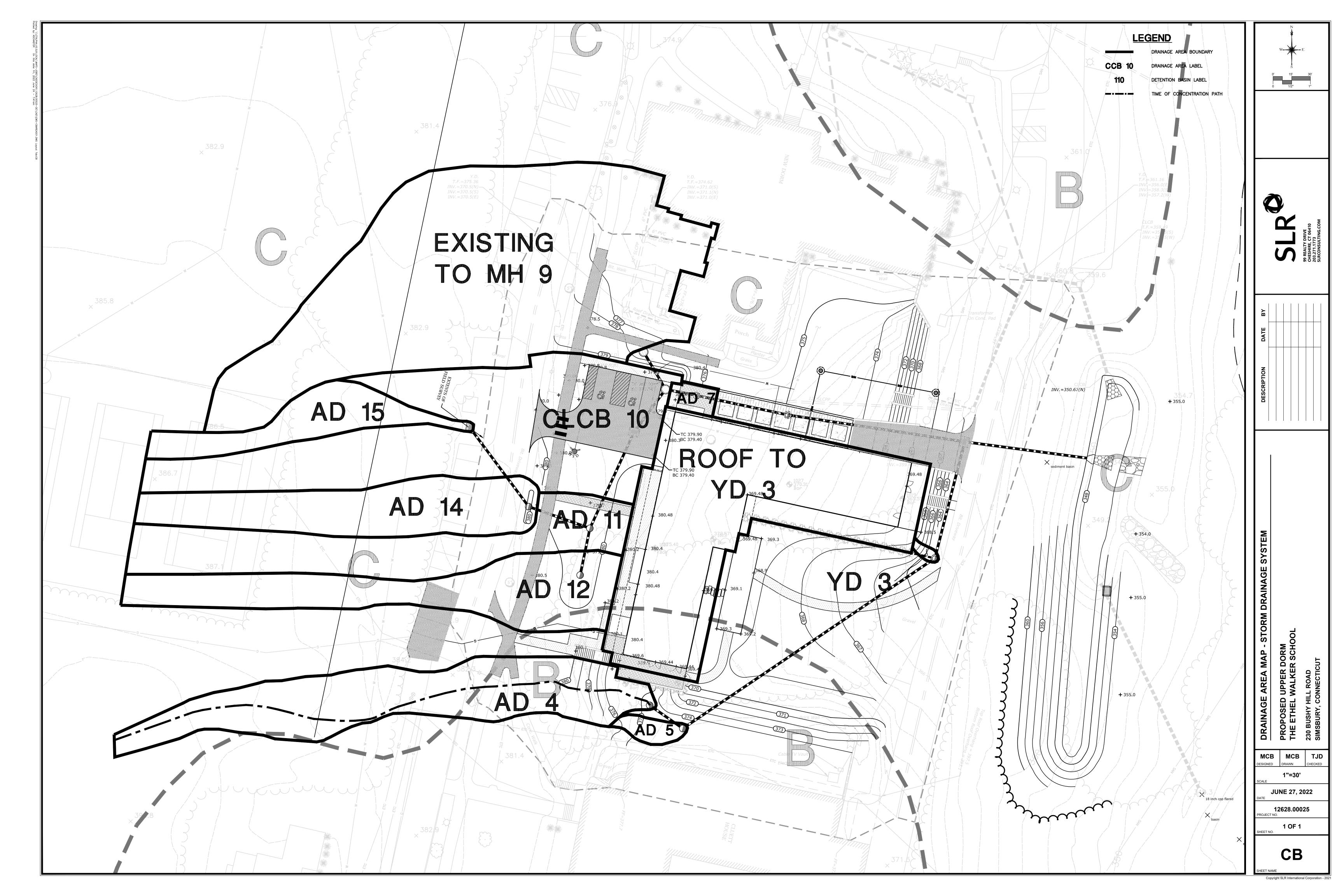
Line		Align	ment			Flov	v Data					Physical	Data				Line ID
No.	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)	
1	End	65.000	-172.407	7 мн	0.00	0.00	0.00	0.0	348.00	4.31	350.80	12	Cir	0.012	0.99	362.90	FES 1 - MH 2
2	1	93.000	1.051	мн	0.00	0.00	0.00	0.0	359.40	7.42	366.30	12	Cir	0.012	0.15	379.50	MH 2 - MH 6
3	2	48.000	3.352	DrGrt	0.00	0.01	0.82	5.0	368.00	1.87	368.90	12	Cir	0.012	0.50	380.30	MH 6 - AD 7
4	3	14.000	-0.674	мн	0.00	0.00	0.00	0.0	368.90	2.14	369.20	12	Cir	0.012	0.92	380.00	AD 7 - MH 8
5	4	27.000	-64.912	Grate	0.00	0.29	0.56	5.0	373.90	1.85	374.40	12	Cir	0.012	0.50	379.10	MH 8 - CLCB 10
6	5	55.000	-11.765	DrGrt	0.00	0.06	0.45	5.0	374.40	1.45	375.20	12	Cir	0.012	2.02	379.40	CLCB 10 - AD 11
7	6	34.000	84.780	DrGrt	0.00	0.12	0.54	5.0	375.80	1.76	376.40	12	Cir	0.012	0.92	379.90	AD 11 - AD 14
8	7	52.000	33.883	DrGrt	0.00	0.06	0.45	5.0	376.40	3.85	378.40	12	Cir	0.012	1.00	381.90	AD 14 - AD 15
9	6	25.000	-12.862	DrGrt	0.00	0.14	0.50	5.0	375.20	1.20	375.50	12	Cir	0.012	1.00	379.30	AD 11 - AD 12
10	1	61.000	-83.265	DrGrt	0.00	0.01	0.30	5.0	358.00	2.46	359.50	12	Cir	0.012	1.07	364.50	MH 2 - YD 3
11	10	161.000			0.00	0.17	0.35	18.5	360.50	3.42	366.00	12	Cir	0.012	1.42	374.50	YD 3 - AD 4
12	11	20.000	69.046	DrGrt	0.00	0.01	0.30	5.0	370.00	5.00	371.00	12	Cir	0.012	1.00	374.50	AD 4 - AD 5
13	4	21.000	48.309	мн	1.86	0.00	0.00	0.0	369.20	1.90	369.60	12	Cir	0.012	1.00	377.50	MH 8 - MH 9
Project	t File: Sys	stem 100-02.	.stm									Number	of lines: 13			Date: 6	/10/2022

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	С	Тс			Total	Сар	Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
Line	То		Incr	Total	coeff	Incr	Total	Inlet	Syst	-(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	-
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	65.000	0.00	0.87	0.00	0.00	0.42	0.0	19.6	4.5	3.76	8.01	4.79	12	4.31	348.00	350.80	353.60	354.22	351.10	362.90	FES 1 - MH 2
2	1	93.000	0.00	0.68	0.00	0.00	0.36	0.0	6.2	8.2	4.82	10.51	9.76	12	7.42	359.40	366.30	359.88	367.21	362.90	379.50	MH 2 - MH 6
3	2	48.000	0.01	0.68	0.82	0.01	0.36	5.0	6.1	8.3	4.84	5.28	7.05	12	1.87	368.00	368.90	368.75	369.81	379.50	380.30	MH 6 - AD 7
4	3	14.000	0.00	0.67	0.00	0.00	0.35	0.0	6.1	8.3	4.78	5.65	6.39	12	2.14	368.90	369.20	369.81	370.10	380.30	380.00	AD 7 - MH 8
5	4	27.000	0.29	0.67	0.56	0.16	0.35	5.0	6.0	8.4	2.94	5.25	5.81	12	1.85	373.90	374.40	374.44	375.13	380.00	379.10	MH 8 - CLCB 10
6	5	55.000	0.06	0.38	0.45	0.03	0.19	5.0	5.7	8.6	1.61	4.65	3.18	12	1.45	374.40	375.20	375.13	375.74	379.10	379.40	CLCB 10 - AD 11
7	6	34.000	0.12	0.18	0.54	0.06	0.09	5.0	5.6	8.6	0.79	5.13	3.86	12	1.76	375.80	376.40	376.07	376.77	379.40	379.90	AD 11 - AD 14
8	7	52.000	0.06	0.06	0.45	0.03	0.03	5.0	5.0	9.0	0.24	7.57	1.53	12	3.85	376.40	378.40	376.77	378.60	379.90	381.90	AD 14 - AD 15
9	6	25.000	0.14	0.14	0.50	0.07	0.07	5.0	5.0	9.0	0.63	4.23	2.13	12	1.20	375.20	375.50	375.74	375.83	379.40	379.30	AD 11 - AD 12
10	1	61.000	0.01	0.19	0.30	0.00	0.07	5.0	19.3	4.5	0.30	6.05	3.12	12	2.46	358.00	359.50	358.15	359.72	362.90	364.50	MH 2 - YD 3
11	10	161.000	0.17	0.18	0.35	0.06	0.06	18.5	18.5	4.6	0.29	7.13	3.34	12	3.42	360.50	366.00	360.64	366.22	364.50	374.50	YD 3 - AD 4
12	11	20.000	0.01	0.01	0.30	0.00	0.00	5.0	5.0	9.0	0.03	8.63	1.84	12	5.00	370.00	371.00	370.04	371.07	374.50	374.50	AD 4 - AD 5
13	4	21.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	1.86	5.32	3.21	12	1.90	369.20	369.60	370.10	370.18	380.00	377.50	MH 8 - MH 9
Proje	ct File:	System	100-02	.stm												Numbe	r of lines: 1	3		Run Da	te: 6/10/20	022
NOT	DTES:Intensity = 43.36 / (Inlet time + 3.80) ^ 0.72; Return period =Yrs. 25 ; c = cir e = ellip b = box																					

Hydraulic Grade Line Computations

.ine	Size	Q			D	ownstr	eam				Len				Upst	ream				Chec	k	JL	Mino
	(in)	(cfs)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	(ft)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)		Ave Sf (%)	Enrgy Ioss (ft)	- coeff (K)	loss (ft)
1	12	3.76	348.00	353.60	1.00	0.79	4.79	0.36	353.96	0.949	65.000	350.80	354.22	1.00	0.79	4.78	0.36	354.57	0.949	0.949	0.617	0.99	0.35
2	12	4.82	359.40	359.88	0.48*	0.37	13.08	0.64	360.52	0.000	93.000	366.30	367.21	0.91**	0.75	6.44	0.64	367.85	0.000	0.000	n/a	0.15	0.10
3	12	4.84	368.00	368.75	0.75*	0.63	7.63	0.65	369.40	0.000	48.000	368.90	369.81	0.91**	0.75	6.47	0.65	370.46	0.000	0.000	n/a	0.50	n/a
4	12	4.78	368.90	369.81	0.91	0.75	6.38	0.64	370.45	0.000	14.000	369.20	370.10 j	0.90**	0.75	6.40	0.64	370.74	0.000	0.000	n/a	0.92	0.59
5	12	2.94	373.90	374.44	0.54*	0.43	6.87	0.35	374.79	0.000	27.000	374.40	375.13	0.73**	0.62	4.75	0.35	375.49	0.000	0.000	n/a	0.50	0.18
6	12	1.61	374.40	375.13	0.73	0.43	2.61	0.22	375.35	0.000	55.000	375.20	375.74 j	0.54**	0.43	3.74	0.22	375.96	0.000	0.000	n/a	2.02	0.44
7	12	0.79	375.80	376.07	0.27*	0.17	4.74	0.14	376.20	0.000	34.000	376.40	376.77	0.37**	0.27	2.98	0.14	376.91	0.000	0.000	n/a	0.92	0.13
8	12	0.24	376.40	376.77	0.37	0.11	0.92	0.07	376.84	0.000	52.000	378.40	378.60 j	0.20**	0.11	2.14	0.07	378.67	0.000	0.000	n/a	1.00	n/a
9	12	0.63	375.20	375.74	0.54	0.23	1.47	0.12	375.86	0.000	25.000	375.50	375.83 j	0.33**	0.23	2.79	0.12	375.95	0.000	0.000	n/a	1.00	n/a
10	12	0.30	358.00	358.15	0.15*	0.07	3.99	0.08	358.23	0.000	61.000	359.50	359.72	0.22**	0.13	2.25	0.08	359.80	0.000	0.000	n/a	1.07	n/a
11	12	0.29	360.50	360.64	0.14*	0.07	4.44	0.08	360.72	0.000	161.00	0366.00	366.22	0.22**	0.13	2.24	0.08	366.30	0.000	0.000	n/a	1.42	n/a
12	12	0.03	370.00	370.04	0.04*	0.01	2.48	0.02	370.06	0.000	20.000	371.00	371.07	0.07**	0.02	1.21	0.02	371.09	0.000	0.000	n/a	1.00	n/a
13	12	1.86	369.20	370.10	0.90	0.47	2.49	0.24	370.34	0.000	21.000	369.60	370.18 j	0.58**	0.47	3.93	0.24	370.42	0.000	0.000	n/a	1.00	n/a
Proje	ect File:	_ System 1	 00-02.stm						1			1	<u> </u>	N	umber o	of lines: 1	3	1	Rur	Date: 6	6/10/202	2	
Note	es:* dent	h assum	ed: ** Criti	cal denth ·	i-Line co	ntains h	vd. jump	; c = c	ir e = ellip	b = box													





APPENDIX E

WATER QUALITY COMPUTATIONS

Drainage Report

Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

June 27, 2022

STORMWATER QUALITY CALCULATIONS Water Quality Volume (WQV)

Basin ID	Post-Development Impervious Area (ac.)	Total Area (ac.)	Percent Impervious	Volumetric Runoff Coeff., R	Recharge Depth ^{1.} , D (in.)	WQV (ac-ft)	GRV (ac-ft)	Total Volume Required ^{2.} (ac-ft)	Total Volume Provided ^{1.} (ac-ft)
110	1.63	4.71	35%	0.36	0.35	0.142	0.016	0.142	0.144

1.- Depth of Runoff to be Recharged or Recharge Depth taken from Table 7-4 found on page 7-6 of the CT DEEP Stormwater Quality

^{2.-} GRV is considered as part of the total WQV required.

$$WQV = \frac{(1.0 \text{ inches}) \text{ x A x R}}{12}$$

Where: WQV = Water Quality Volume in acre-feet A = Contributing Area in acres R = 0.05 + 0.009 (I) I = Site Imperviousness as percent

$$\mathbf{GRV} = \frac{\mathbf{D} \mathbf{x} \mathbf{A} \mathbf{x} \mathbf{I}}{12}$$

Where: GRV = Groundwater Recharge Volume in acre-feet

D = Depth of Runoff to be Recharged in inches

A = Contributing Area in acres

STORMWATER QUALITY CALCULATIONS Water Quality Volume (WQV)

<u>DET 110</u>

Elevation (ft)	Surface Area (ft2)	Volume (ft3)	Volume (ac-ft)	Cumulative Volume (ac-ft)
348.0	2,485	0.0	0.000	0.000
349.0	3,345	2,915.0	0.067	0.067
349.9	4,119	3,358.8	0.077	0.144





APPENDIX F

HYDROLOGIC ANALYSIS – INPUT COMPUTATIONS

Drainage Report

Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

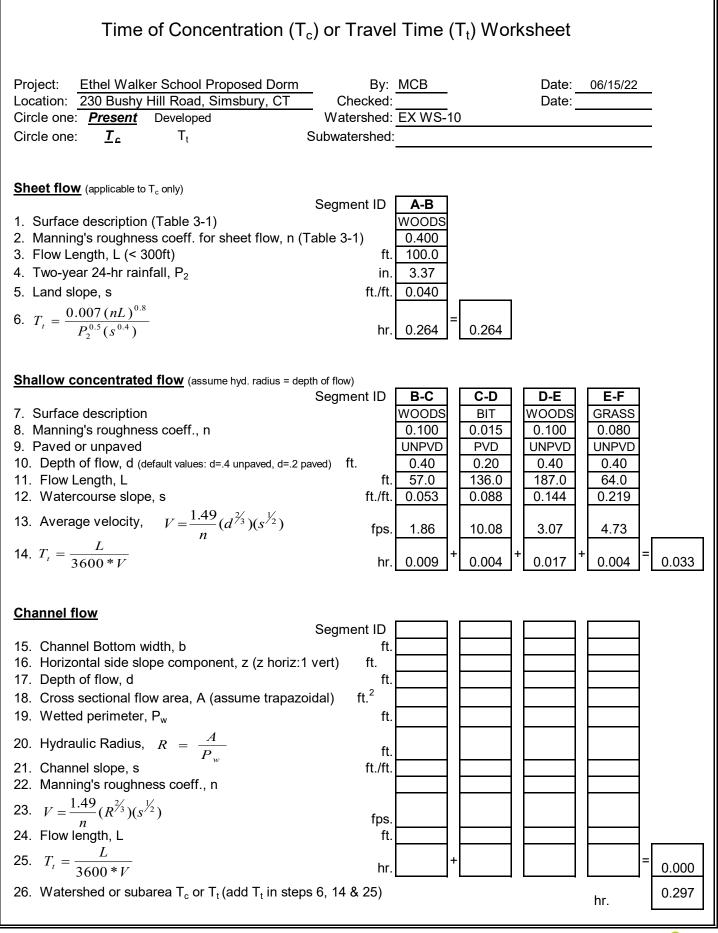
June 27, 2022

	Curve Number Ca	alcula	ation	S		
Location:		- necked: ershed:		- 	Date:	
Soil Name and Hydrologic Group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Area Acres Sq. Ft. %	Product of CN x Area
B Soil	Woods - Good Condition	55			0.19	10.48
B Soil	Open Space - Good Condition	61			0.39	23.59
B Soil	Gravel	85			0.01	0.44
C Soil	Woods - Good Condition	70			1.14	79.83
C Soil	Open Space - Good Condition	74			1.68	124.33
C Soil	Gravel	89			0.03	2.96
N/A	Building	98			0.28	27.38
N/A	Paved/Impervious	98			0.79	77.50
<u></u>		1	Tota	als = (4.51 0.00704	346.51 sq mi)
CN (6.51 .51	Use	e CN =	77]

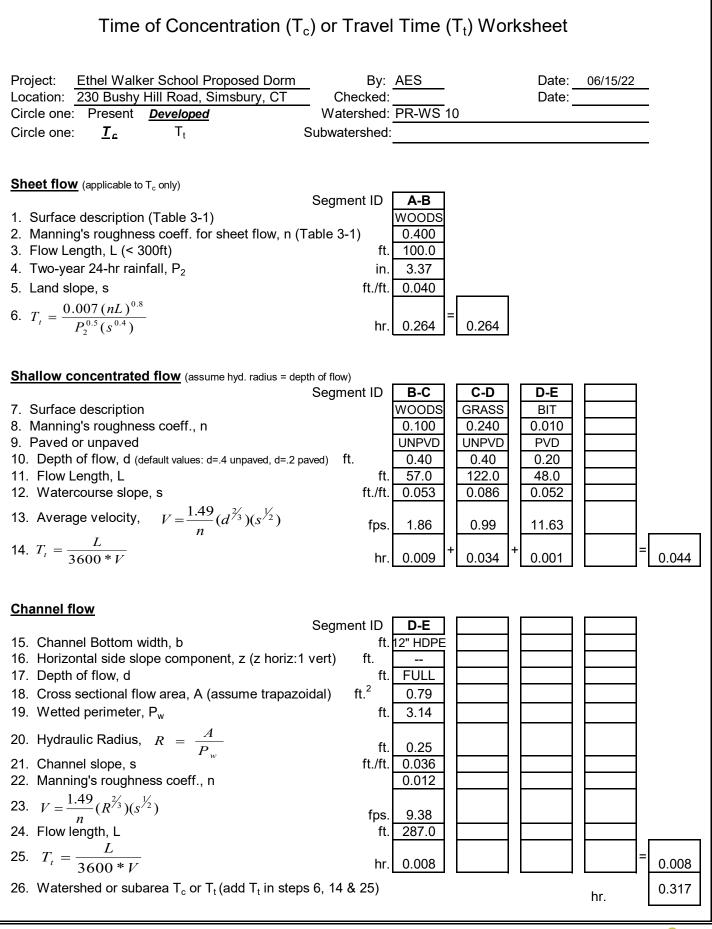


	Curve Number Ca	alcula	ation	S		
Location:		- hecked: ershed:		5 10	Date:	
Soil Name and Hydrologic Group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Area Acres Sq. Ft. %	Product of CN x Area
B Soil	Woods - Good Condition	55			0.03	1.71
B Soil	Open Space - Good Condition	61			0.49	29.94
B Soil	Gravel	85			0.01	0.44
C Soil	Woods - Good Condition	70			0.98	68.70
C Soil	Open Space - Good Condition	74			1.61	119.41
C Soil	Gravel	89			0.01	0.81
N/A	Building	98			0.58	57.15
N/A	Paved/Impervious	98			1.03	100.71
			Tota	als = (4.74 0.00741	378.88 sq mi)
CN (¹		3.88 74	Use	e CN =	80]









SLR

Precipitation Frequency Data Server



NOAA Atlas 14, Volume 10, Version 3 Location name: Simsbury, Connecticut, USA* Latitude: 41.8484°, Longitude: -72.833° Elevation: 345.08 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-	S-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹													
Duration				Average I	recurrence	interval (y	ears)							
Duration	1	2	5	10	25	50	100	200	500	1000				
5-min	0.351 (0.270-0.451)	0.420 (0.323-0.541)	0.533 (0.408-0.688)	0.626 (0.477-0.814)	0.755 (0.558-1.03)	0.852 (0.618-1.19)	0.953 (0.673-1.38)	1.07 (0.715-1.59)	1.23 (0.793-1.89)	1.36 (0.858-2.14)				
10-min	0.497 (0.382-0.639)	0.595 (0.457-0.766)	0.755 (0.578-0.976)	0.887 (0.676-1.15)	1.07 (0.791-1.46)	1.21 (0.875-1.68)	1.35 (0.953-1.96)	1.51 (1.01-2.25)	1.74 (1.13-2.69)	1.92 (1.22-3.03)				
15-min	0.585 (0.450-0.752)	0.700 (0.538-0.901)	0.888 (0.680-1.15)	1.04 (0.795-1.36)	1.26 (0.930-1.71)	1.42 (1.03-1.98)	1.59 (1.12-2.30)	1.78 (1.19-2.64)	2.04 (1.32-3.16)	2.26 (1.43-3.57)				
30-min	0.791 (0.609-1.02)	0.949 (0.730-1.22)	1.21 (0.925-1.56)	1.42 (1.08-1.85)	1.72 (1.27-2.34)	1.94 (1.41-2.70)	2.17 (1.53-3.15)	2.43 (1.63-3.61)	2.79 (1.81-4.32)	3.09 (1.96-4.88)				
60-min	0.998 (0.768-1.28)	1.20 (0.921-1.54)	1.53 (1.17-1.97)	1.80 (1.37-2.34)	2.17 (1.61-2.96)	2.46 (1.78-3.43)	2.75 (1.94-3.99)	3.08 (2.07-4.58)	3.54 (2.29-5.48)	3.92 (2.48-6.19)				
2-hr	1.29 (0.997-1.65)	1.54 (1.19-1.97)	1.96 (1.51-2.51)	2.30 (1.77-2.98)	2.78 (2.07-3.77)	3.13 (2.29-4.36)	3.51 (2.50-5.10)	3.95 (2.66-5.86)	4.61 (3.00-7.11)	5.17 (3.28-8.14)				
3-hr	1.48 (1.15-1.89)	1.78 (1.38-2.27)	2.26 (1.75-2.90)	2.67 (2.05-3.43)	3.22 (2.41-4.37)	3.63 (2.67-5.05)	4.07 (2.93-5.93)	4.61 (3.11-6.81)	5.42 (3.53-8.33)	6.12 (3.90-9.61)				
6-hr	1.87 (1.46-2.36)	2.26 (1.77-2.86)	2.91 (2.27-3.70)	3.44 (2.67-4.41)	4.18 (3.15-5.65)	4.72 (3.50-6.56)	5.32 (3.86-7.74)	6.06 (4.10-8.92)	7.22 (4.71-11.0)	8.22 (5.25-12.8)				
12-hr	2.30 (1.81-2.88)	2.83 (2.23-3.56)	3.70 (2.90-4.67)	4.42 (3.45-5.62)	5.41 (4.11-7.29)	6.14 (4.59-8.51)	6.95 (5.08-10.1)	7.97 (5.41-11.7)	9.57 (6.26-14.6)	11.0 (7.03-17.1)				
24-hr	2.68 (2.13-3.35)	3.37 (2.67-4.21)	4.50 (3.55-5.64)	5.43 (4.27-6.86)	6.72 (5.14-9.03)	7.66 (5.77-10.6)	8.71 (6.43-12.7)	10.1 (6.86-14.7)	12.3 (8.05-18.6)	14.2 (9.13-22.0)				
2-day	3.01 (2.40-3.73)	3.85 (3.07-4.78)	5.23 (4.16-6.51)	6.37 (5.04-7.99)	7.94 (6.13-10.6)	9.08 (6.90-12.6)	10.4 (7.75-15.2)	12.1 (8.29-17.6)	15.0 (9.89-22.7)	17.7 (11.4-27.2)				
3-day	3.28 (2.63-4.04)	4.20 (3.37-5.20)	5.72 (4.57-7.10)	6.98 (5.54-8.72)	8.71 (6.75-11.7)	9.96 (7.61-13.7)	11.4 (8.55-16.6)	13.3 (9.14-19.3)	16.6 (10.9-25.0)	19.6 (12.6-30.1)				
4-day	3.52 (2.84-4.34)	4.51 (3.63-5.57)	6.14 (4.91-7.59)	7.48 (5.96-9.32)	9.33 (7.25-12.4)	10.7 (8.16-14.7)	12.2 (9.17-17.8)	14.3 (9.79-20.6)	17.8 (11.7-26.7)	20.9 (13.5-32.2)				
7-day	4.22 (3.41-5.16)	5.33 (4.31-6.54)	7.16 (5.77-8.81)	8.67 (6.94-10.7)	10.8 (8.40-14.3)	12.3 (9.42-16.8)	14.0 (10.5-20.2)	16.3 (11.2-23.5)	20.1 (13.3-30.2)	23.6 (15.3-36.1)				
10-day	4.91 (3.99-5.98)	6.08 (4.94-7.43)	8.01 (6.48-9.82)	9.61 (7.72-11.9)	11.8 (9.24-15.6)	13.4 (10.3-18.2)	15.2 (11.4-21.8)	17.6 (12.2-25.3)	21.6 (14.3-32.2)	25.1 (16.3-38.3)				
20-day	7.08 (5.79-8.57)	8.30 (6.78-10.1)	10.3 (8.39-12.6)	12.0 (9.68-14.7)	14.3 (11.2-18.5)	15.9 (12.3-21.3)	17.8 (13.3-25.1)	20.2 (14.0-28.7)	23.9 (16.0-35.5)	27.2 (17.7-41.4)				
30-day	8.90 (7.31-10.7)	10.1 (8.32-12.3)	12.2 (9.95-14.8)	13.9 (11.3-16.9)	16.2 (12.7-20.8)	17.9 (13.8-23.7)	19.7 (14.7-27.4)	22.0 (15.4-31.2)	25.4 (17.0-37.6)	28.4 (18.5-43.0)				
45-day	11.2 (9.21-13.4)	12.4 (10.2-15.0)	14.5 (11.9-17.5)	16.3 (13.3-19.8)	18.6 (14.7-23.8)	20.4 (15.7-26.7)	22.3 (16.5-30.4)	24.4 (17.1-34.4)	27.3 (18.3-40.3)	29.7 (19.4-44.9)				
60-day	13.0 (10.8-15.6)	14.4 (11.9-17.2)	16.5 (13.6-19.9)	18.3 (15.0-22.2)	20.8 (16.4-26.4)	22.7 (17.4-29.5)	24.6 (18.2-33.2)	26.5 (18.7-37.3)	29.0 (19.5-42.6)	30.9 (20.2-46.6)				

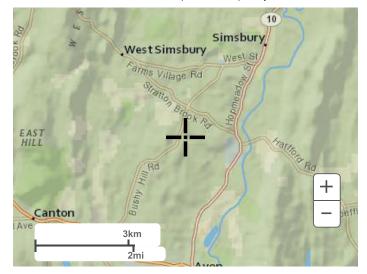
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

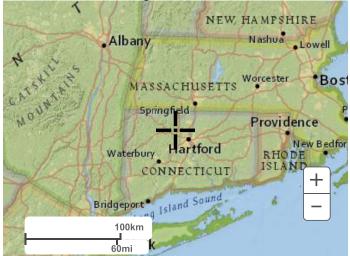
Back to Top

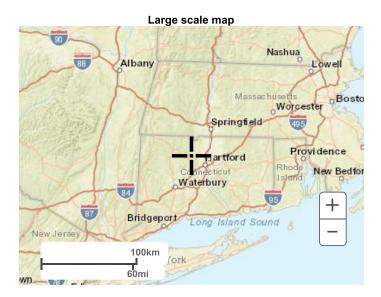
PF graphical

Precipitation Frequency Data Server



Large scale terrain





Large scale aerial



APPENDIX G

HYDROLOGIC ANALYSIS – COMPUTER MODEL RESULTS

Drainage Report

Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

June 27, 2022

Hydrographs Peak Flowrate Summary (cfs) Existing vs. Proposed

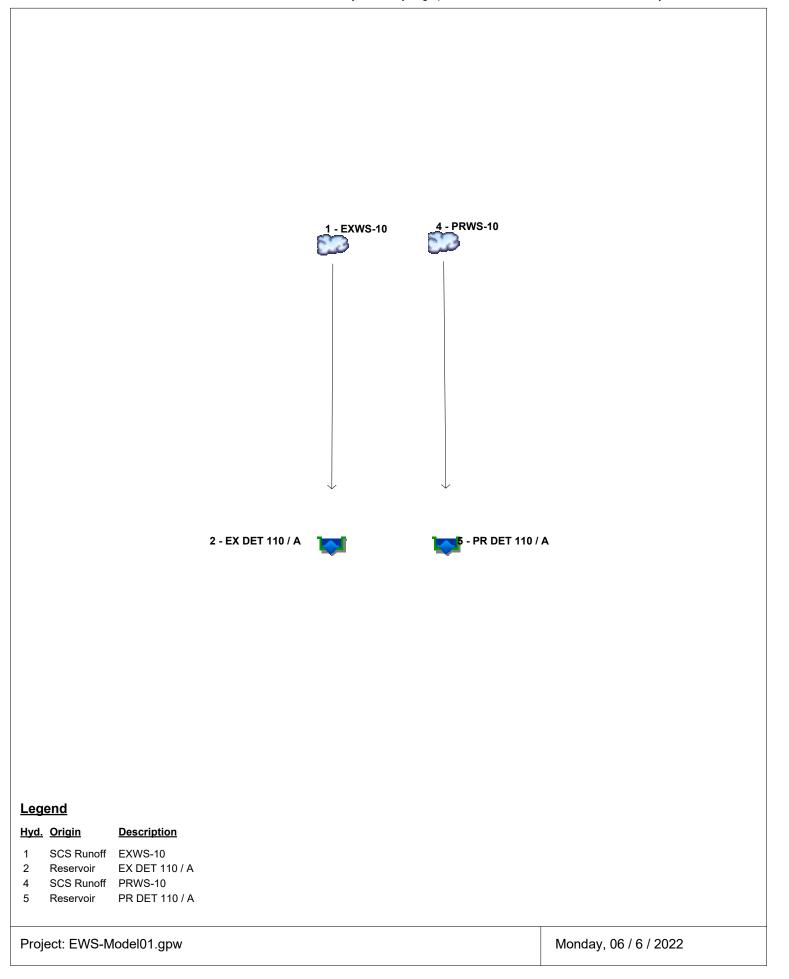
Storm Event	2yr		10yr		25yr		50yr		100yr	
Storm Event	Exist	Prop								
Point of Analysis A	2.7	2.7	10.1	5.5	14.7	12.1	17.2	16.6	21.0	19.1
DET 110 W.S. Elev. (ft.) Top of Berm Elev.=354.7 Top of Berm Elev.=355.0	352.2	351.5	353.2	353.1	353.4	353.6	353.6	353.7	353.8	354.0

Study Area

Description

Α

Outflow from Detention Basin



Hydraflow Table of Contents

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020	Monday, 06 / 6 / 2022
Watershed Model Schematic	1
Hydrograph Return Period Recap	2
2 - Year Summary Report	3
10 - Year Summary Report	4
25 - Year Summary Report	5
50 - Year Summary Report	6
100 - Year Summary Report	

Hydrograph Return Period Recap Hydraffow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

lo.	Hydrograph	Inflow byd(s)				Hydrograph Description					
10.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			4.901			11.28	15.54	18.70	22.25	EXWS-10
2	Reservoir	1		2.730			10.06	14.72	17.20	21.00	EX DET 110 / A
4	SCS Runoff			6.008			12.99	17.54	20.89	24.63	PRWS-10
5	Reservoir	4		2.738			5.476	12.09	16.63	19.12	PR DET 110 / A

lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description
1	SCS Runoff	4.901	3	735	0.517				EXWS-10
2	Reservoir	2.730	3	753	0.503	1	352.17	0.149	EX DET 110 / A
4	SCS Runoff	6.008	3	732	0.625				PRWS-10
5	Reservoir	2.738	3	756	0.616	4	351.54	0.329	PR DET 110 / A
EWS-Model01.gpw						Period: 2 Ye			6 / 6 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description
1	SCS Runoff	11.28	3	732	1.158				EXWS-10
2	Reservoir	10.06	3	741	1.143	1	353.16	0.234	EX DET 110 / A
4	SCS Runoff	12.99	3	732	1.332				PRWS-10
5	Reservoir	5.476	3	753	1.324	4	353.05	0.545	PR DET 110 / A
ΕW	EWS-Model01.gpw					Period: 10 `	Year	Monday, 0	6 / 6 / 2022

łyd. lo.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description
1	SCS Runoff	15.54	3	732	1.595				EXWS-10
2	Reservoir	14.72	3	738	1.581	1	353.37	0.254	EX DET 110 / A
4	SCS Runoff	17.54	3	732	1.807				PRWS-10
5	Reservoir	12.09	3	747	1.799	4	353.57	0.634	PR DET 110 / A
EW	WS-Model01.gpw				Return	Period: 25 `	Year	Monday, 0	6 / 6 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description
1	SCS Runoff	18.70	3	732	1.924				EXWS-10
2	Reservoir	17.20	3	738	1.910	1	353.60	0.278	EX DET 110 / A
4	SCS Runoff	20.89	3	732	2.162				PRWS-10
5	Reservoir	16.63	3	741	2.153	4	353.73	0.662	PR DET 110 / A

lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description
1	SCS Runoff	22.25	3	732	2.298				EXWS-10
2	Reservoir	21.00	3	738	2.284	1	353.80	0.296	EX DET 110 / A
4	SCS Runoff	24.63	3	732	2.564				PRWS-10
5	Reservoir	19.12	3	744	2.555	4	353.99	0.707	PR DET 110 / A
	/S-Model01.g				Deturn	Period: 100		Mardau	6 / 6 / 2022

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Pond No. 1 - EX DET 110

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 349.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	349.00	540	0.000	0.000
1.00	350.00	1,582	0.023	0.023
2.00	351.00	2,463	0.046	0.069
3.00	352.00	3,344	0.066	0.136
4.00	353.00	3,944	0.084	0.219
5.00	354.00	4,544	0.097	0.317
5.70	354.70	5,813	0.083	0.400

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 18.00	4.00	0.00	0.00	Crest Len (ft)	= 12.70	0.00	10.00	0.00
Span (in)	= 18.00	4.00	0.00	0.00	Crest El. (ft)	= 353.00	350.60	353.50	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	0.68	2.60	3.33
Invert El. (ft)	= 349.00	349.60	0.00	0.00	Weir Type	= Rect	30 degV	Broad	
Length (ft)	= 69.00	0.00	0.00	0.00	Multi-Stage	= Yes	Yes	No	No
Slope (%)	= 1.44	0.00	0.00	n/a					
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Weir Structures

Stage /	Stage / Storage / Discharge Table													
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs	
0.00	0.000	349.00	0.00	0.00			0.00		0.00				0.000	
1.00	0.023	350.00	0.20 ic	0.20 ic			0.00		0.00				0.203	
2.00	0.069	351.00	0.55 ic	0.47 ic			0.00	0.07	0.00				0.535	
3.00	0.136	352.00	2.23 ic	0.63 ic			0.00	1.58	0.00				2.207	
4.00	0.219	353.00	6.77 ic	0.68 ic			0.00	6.08	0.00				6.758	
5.00	0.317	354.00	17.46 ic	0.08 ic			14.29 s	3.07 s	9.19				26.64	
5.70	0.400	354.70	18.91 ic	0.05 ic			16.00 s	2.82 s	34.18				53.04	

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Pond No. 2 - PR DET 110

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 348.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	348.00	2,485	0.000	0.000
1.00	349.00	3,345	0.067	0.067
2.00	350.00	4,205	0.086	0.153
3.00	351.00	5,117	0.107	0.260
4.00	352.00	6,028	0.128	0.388
5.00	353.00	7,031	0.150	0.537
6.00	354.00	8,033	0.173	0.710
7.00	355.00	9,000	0.195	0.906

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 18.00	6.00	9.00	0.00	Crest Len (ft)	= 14.00	0.00	10.00	0.00
Span (in)	= 18.00	8.00	9.00	0.00	Crest El. (ft)	= 353.30	0.00	354.00	0.00
No. Barrels	= 1	1	1	0	Weir Coeff.	= 3.33	3.33	2.60	3.33
Invert El. (ft)	= 348.00	349.90	351.00	0.00	Weir Type	= Rect		Broad	
Length (ft)	= 69.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.44	0.00	0.00	n/a	-				
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	Yes	Yes	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

-	-	-											
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0.000	348.00	0.00	0.00	0.00		0.00		0.00				0.000
1.00	0.067	349.00	0.00	0.00	0.00		0.00		0.00				0.000
2.00	0.153	350.00	0.07 ic	0.07 ic	0.00		0.00		0.00				0.072
3.00	0.260	351.00	1.48 ic	1.48 ic	0.00		0.00		0.00				1.480
4.00	0.388	352.00	3.88 ic	2.18 ic	1.68 ic		0.00		0.00				3.865
5.00	0.537	353.00	5.43 ic	2.71 ic	2.71 ic		0.00		0.00				5.421
6.00	0.710	354.00	19.19 ic	0.64 ic	0.85 ic		17.69 s		0.00				19.19
7.00	0.906	355.00	21.24 ic	0.21 ic	0.28 ic		20.73 s		26.00				47.22



APPENDIX H

WATERSHED MAPS

Drainage Report

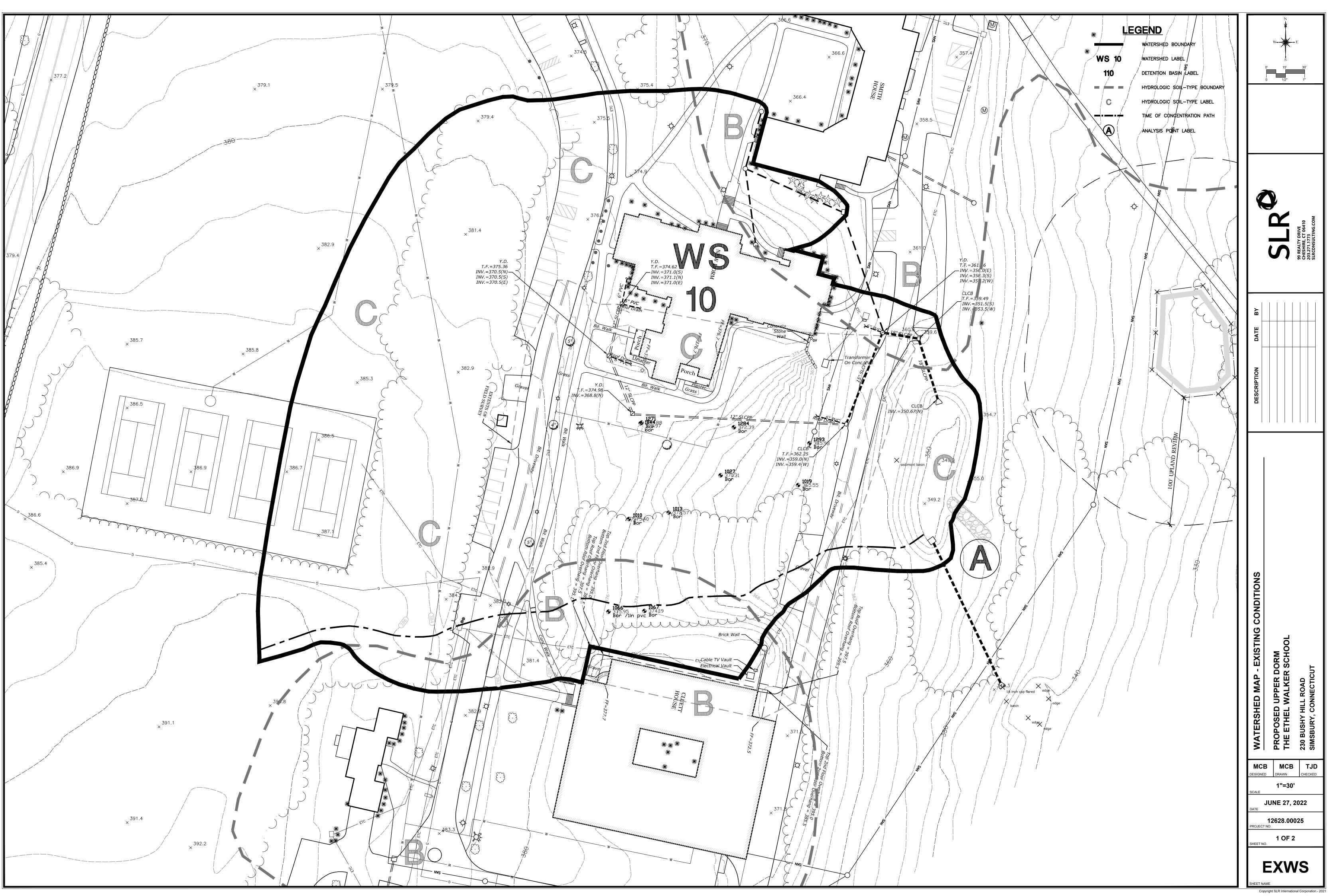
Ethel Walker School

230 Bushy Hill Road

Simsbury, Connecticut 06070

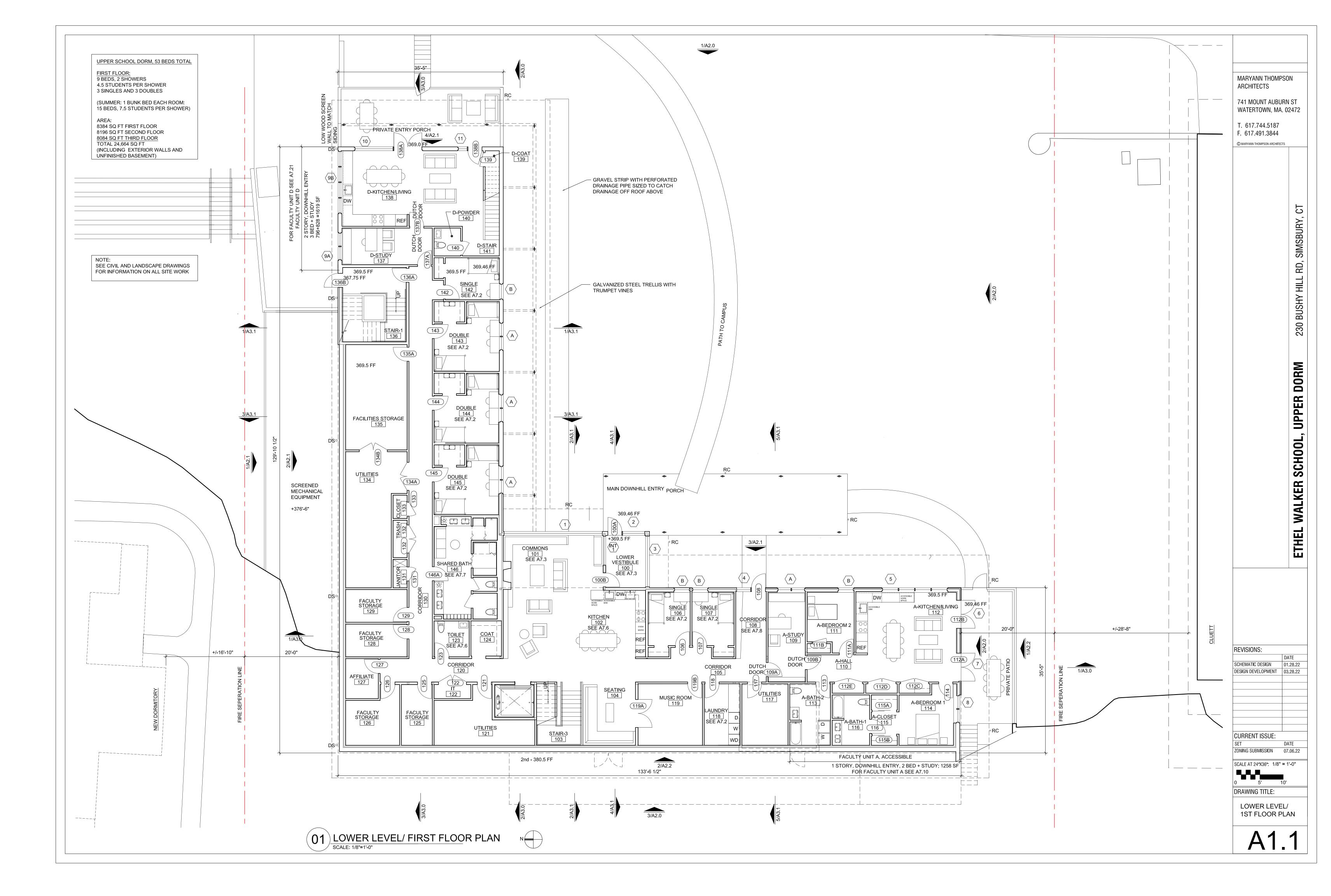
June 27, 2022

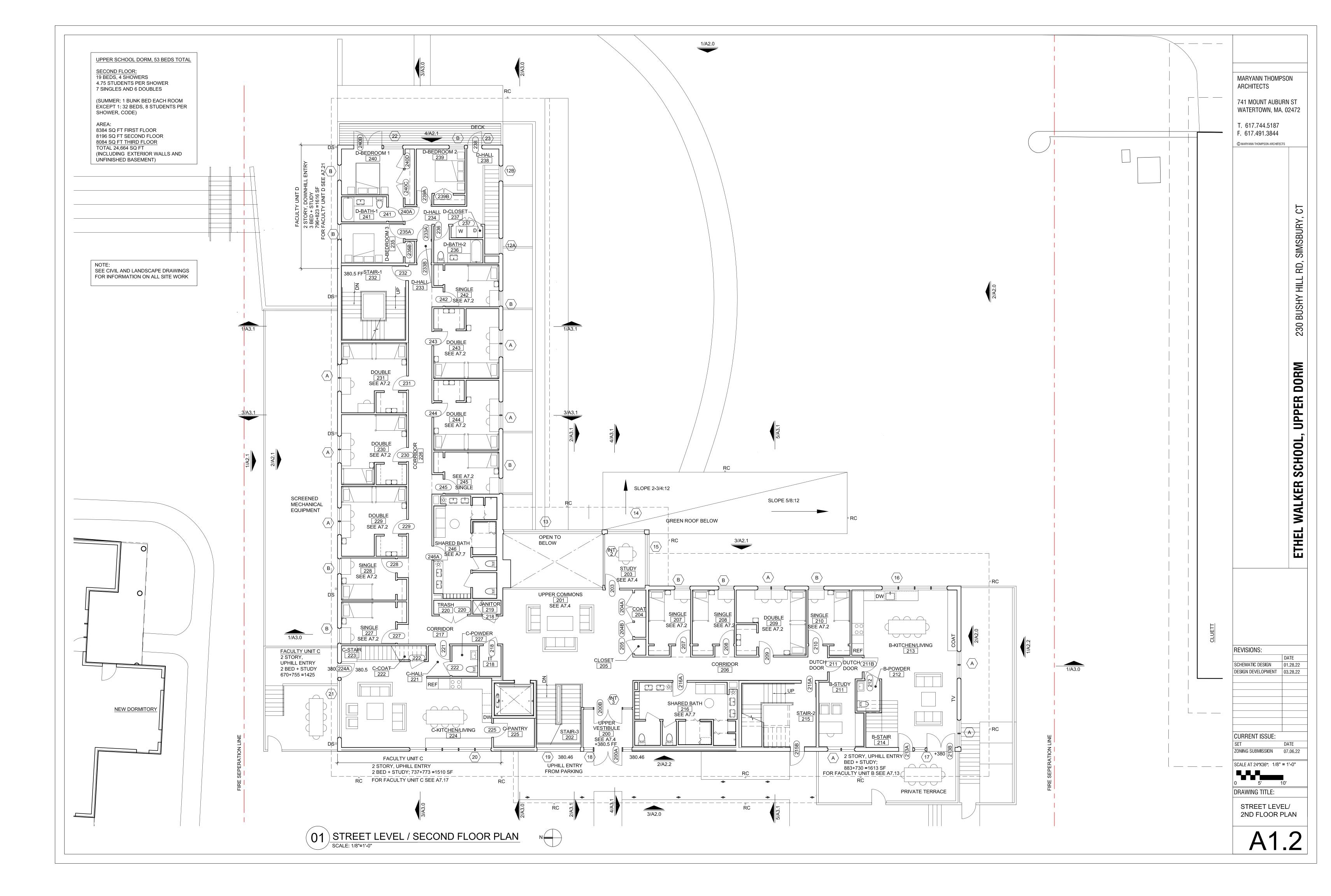














<u>THIRD FLOOR:</u> 25 BEDS, 5 SHOWERS 5 STUDENTS PER SHOWER 9 SINGLES AND 8 DOUBLES

(SUMMER: 1 BUNK BED EACH ROOM EXCEPT 2 SINGLE: 40 BEDS, 8 STUDENTS PER SHOWER, CODE)

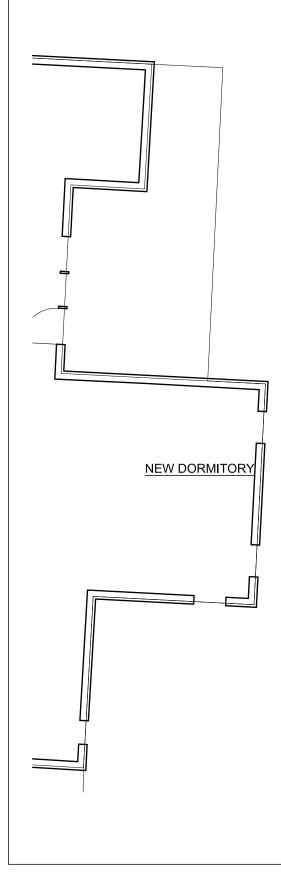
AREA: 9384 SQ FT FIRST FLOOR 8196 SQ FT SECOND FLOOR 8084 SQ FT THIRD FLOOR TOTAL 24,664 SQ FT (INCLUDING EXTERIOR WALLS AND UNFINISHED BASEMENT)

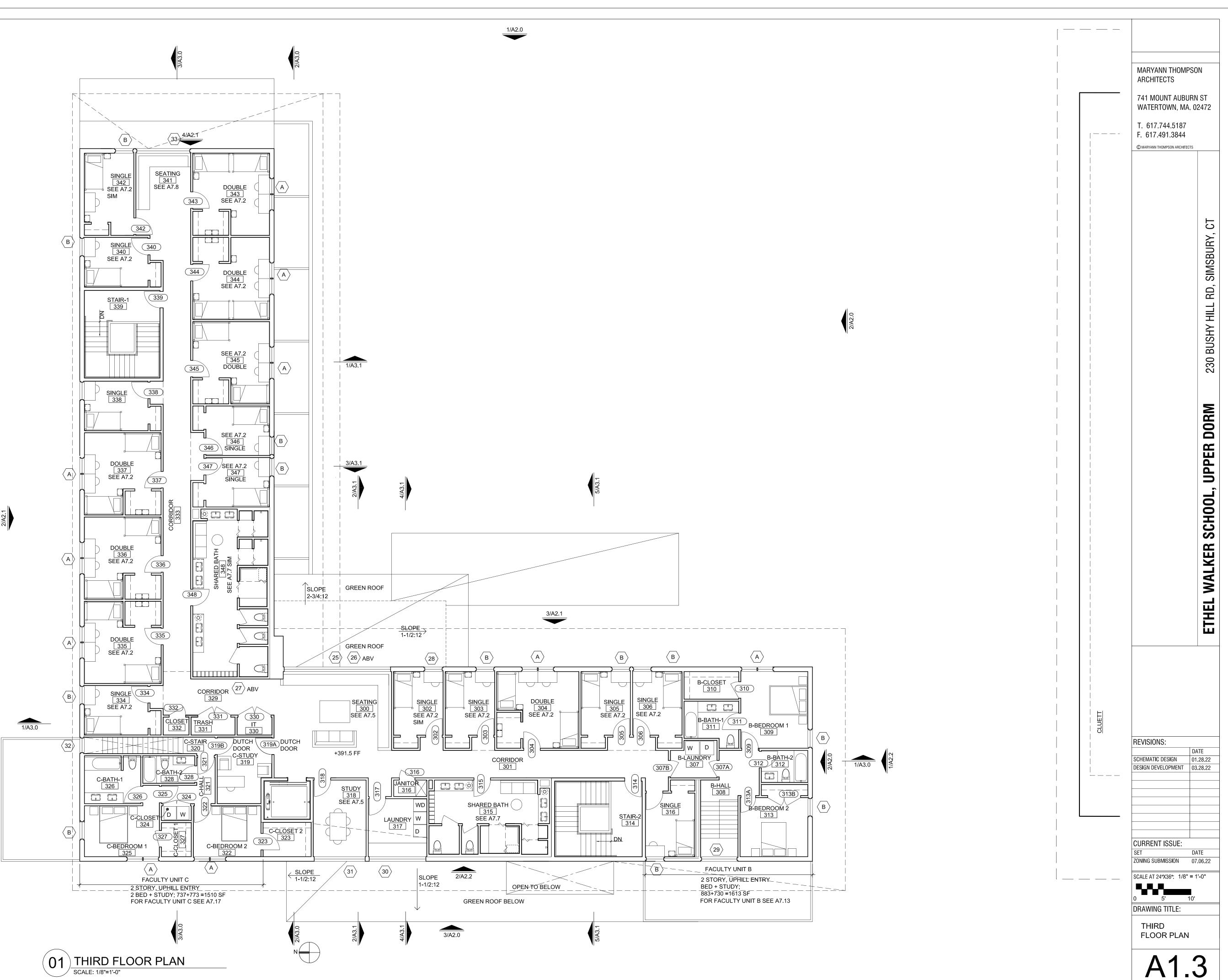
NOTE: SEE CIVIL AND LANDSCAPE DRAWINGS FOR INFORMATION ON ALL SITE WORK

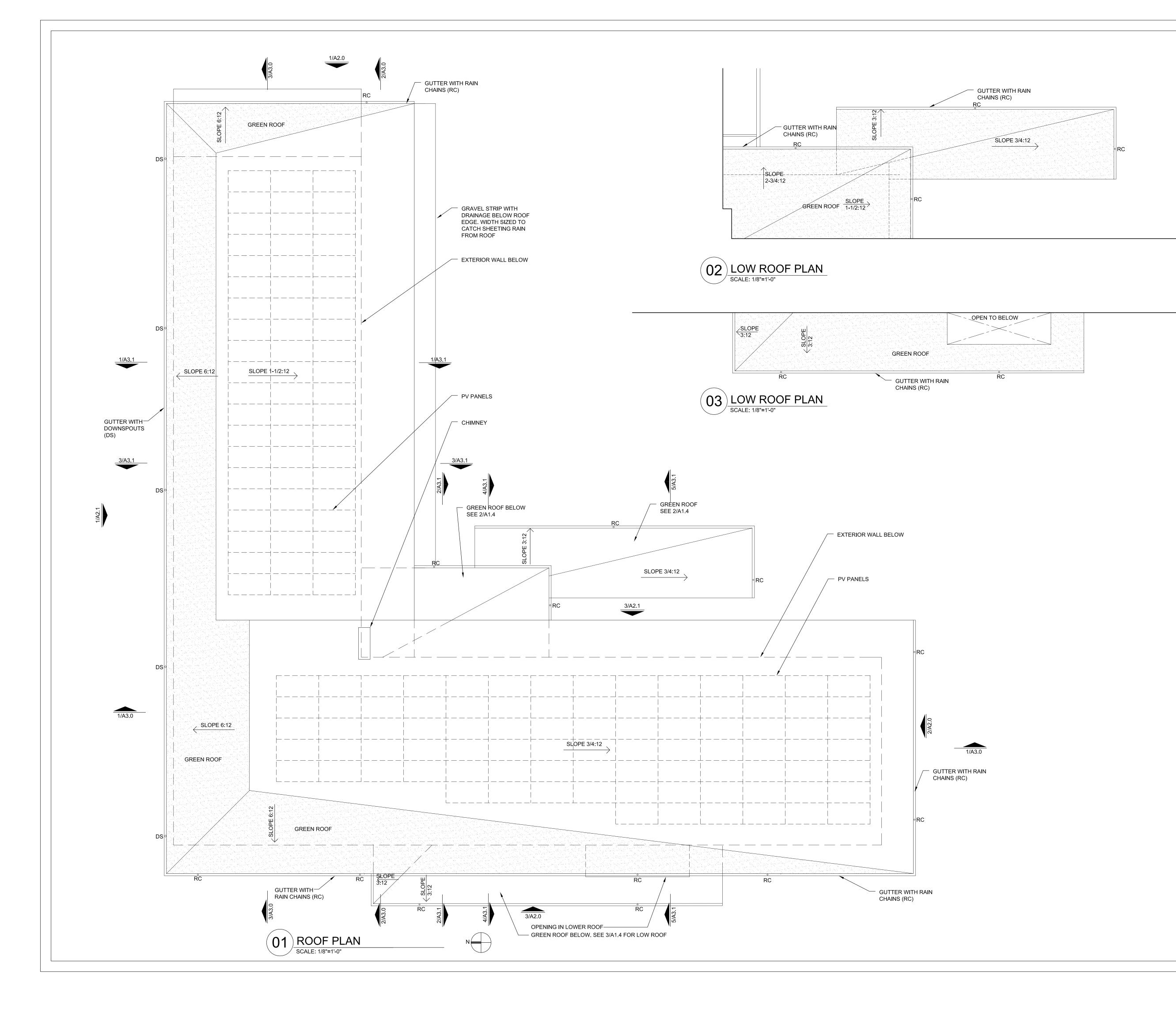
1/A3.1

3/A3.1

A2 1







ARCHITECTS 741 MOUNT AUBURN ST WATERTOWN, MA. 02472 T. 617.744.5187 F. 617.491.3844 © MARYANN THOMPSON ARCHITECTS						
		230 BUSHY HILL RD, SIMSBURY, CT				
		ETHEL WALKER SCHOOL, UPPER DORM				
REVISIONS: SCHEMATIC DESIGN DESIGN DEVELOPMENT	01	TE 28.22 28.22				
CURRENT ISSUE: SET ZONING SUBMISSION SCALE AT 24"X36": 1/8" 0 5' DRAWING TITLE: ROOF PLAN	07	TE .06.22 '-0"				
A1		4				

MARYANN THOMPSON



